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NEW JERSEY DEPT OF ENVIRONMENTAL PROTECTION TRENTON --ETC F/G 13/13
NATIONAL DAM SAFETY PROGRAM. ETRA LAKE DAM (NJ00298), RARITAN R--ETC(U)
JUL 81 J J WILLIAMS DACW61-79-C-0011

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RARITAN RIVER BASIN
ROCKY BROOK, MERCER COUNTY
NEW JERSEY

ETRA LAKE DAM
NJ 00298

PHASE 1 INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

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DEPARTMENT OF THE ARMY

Philadelphia District
Corps of Engineers
Philadelphia, Pennsylvania

JULY 1981

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.		

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Honorable Brendan T. Byrne
Governor of New Jersey
Trenton, New Jersey 08621

11 AUG 1981

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Etra Mill Pond Dam in Mercer County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Etra Mill Pond Dam, initially listed as a high hazard potential structure but reduced to a low hazard potential structure as a result of this inspection, is judged to be in fair overall condition. However, the spillway is considered inadequate, as 23 percent of the 100 year design flood would cause the dam to be overtopped. The low hazard potential classification means that in the event of failure of the dam, no loss of life and only minimal economic loss is expected. For the same reasons no further studies or increase of spillway capacity are recommended. However, to assure the continued functioning of the dam and its impoundment, the following remedial actions could be undertaken by the owner:

- a. Clear the embankment of all brush and trees. Backfill resulting voids with suitable compacted material. Establish controlled protective vegetation on the embankment slopes.
- b. Monitor the seepage downstream of the dam regularly.
- c. Consider increasing the spillway capacity to provide for safe passage of the Spillway Design Flood.
- d. Repair the concrete in the spillway and bridge.
- e. Inspect the reservoir drain and repair if necessary to insure satisfactory operation.

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Honorable Brendan T. Byrne

f. Inspect the diversion system to the former mill to assess its suitability for use as an auxiliary reservoir drain.

g. Develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Smith of the Fourth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,



ROGER L. BALDWIN
Lieutenant Colonel, Corps of Engineers
Commander and District Engineer

I Incl
As stated

Copies furnished:
Mr. Dirk C. Hofman, P.E., Deputy Director
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CNO29
Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief
Bureau of Flood Plain Regulation
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CNO29
Trenton, NJ 08625

ETRA MILL POND DAM (NJ00298)

CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 30 April 1981 and 6 and 13 May 1981 by O'Brien and Gere Engineers Inc. under contract to the U.S. Army Engineer District, Philadelphia, in accordance with the National Dam Inspection Act, Public Law 92-367.

Etra Mill Pond Dam, initially listed as a high hazard potential structure but reduced to a low hazard potential structure as a result of this inspection, is judged to be in fair overall condition. However, the spillway is considered inadequate, as 23 percent of the 100 year design flood would cause the dam to be overtopped. The low hazard potential classification means that in the event of failure of the dam, no loss of life and only minimal economic loss is expected. For the same reasons no further studies or increase of spillway capacity are recommended. However, to assure the continued functioning of the dam and its impoundment, the following remedial actions could be undertaken by the owner:

- a. Clear the embankment of all brush and trees. Backfill resulting voids with suitable compacted material. Establish controlled protective vegetation on the embankment slopes.
- b. Monitor the seepage downstream of the dam regularly.
- c. Consider increasing the spillway capacity to provide for safe passage of the Spillway Design Flood.
- d. Repair the concrete in the spillway and bridge.
- e. Inspect the reservoir drain and repair if necessary to insure satisfactory operation.
- f. Inspect the diversion system to the former mill to assess its suitability for use as an auxiliary reservoir drain.
- g. Develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

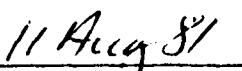
APPROVED:



ROGER L. BALDWIN

Lieutenant Colonel, Corps of Engineers
Commander and District Engineer

DATE:



DELAWARE RIVER BASIN

Name of Dam: Etra Mill Pond
County & State: Mercer County, New Jersey
Inventory Number: NJ 00298

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Prepared by:

O'BRIEN & GERE ENGINEERS, INC.

For

DEPARTMENT OF THE ARMY
Philadelphia District, Corps of Engineers
Custom House-2nd & Chestnut Streets
Philadelphia, PA 19106

August 1981

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I REPORT
NATIONAL DAM INVENTORY PROGRAM

Name of Dam: Etra Mill Pond Dam
State Located: New Jersey
County Located: Mercer
Stream: Rocky Brook
Coordinates: N40°15.2', W74°30.2'
Dates of Inspection: April 30, 1981, May 6, 1981
and May 13, 1981

ASSESSMENT

Etra Mill Pond Dam is an earth embankment about 300 feet long and 11 feet high. The embankment has a crest width of about 25 feet with a paved roadway constructed on it. An Ambursen type reinforced concrete spillway is located at about the midpoint of the dam. The upstream slope of the embankment averages 2H:1V while the downstream slope of the embankment averages 1H:1V.

The dam is classified as "Small" size. Based on the potential for damage due to dam failure, the structure is judged to be a "Low" hazard. Accordingly, the Spillway Design Flood (SDF) range from the fifty-year flood to the one-hundred year flood. The one-hundred year flood was selected as the SDF. The SDF was developed and routed through the structure. Based on a review of the results, the spillway is capable of passing only 22 percent of the SDF without overtopping the embankment. The spillway is classified as "Inadequate".

The Owner should retain the services of a licensed professional engineer experienced in the design and construction of dams to assist in complying with the following recommendations and remedial measures.

The recommendations and remedial measures should be initiated soon.

a. Facilities

1. The embankment should be cleared of all brush and trees. Resulting voids should be backfilled with suitable compacted material. Controlled protective vegetation should be established on the embankment slopes.
2. The seepage downstream of the dam should be monitored regularly.
3. The capacity of the spillway should be increased to provide for safe passage of the SDF.
4. The concrete in the spillway and bridge should be repaired.

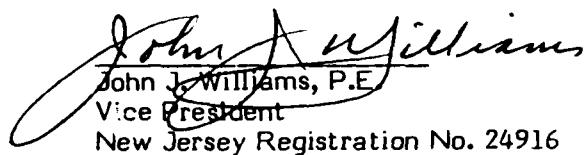
5. The reservoir drain should be inspected and repaired if necessary to insure satisfactory operation.

6. The diversion system to the former mill should be inspected to assess its suitability for use as an auxiliary reservoir drain.

b. Operation and Maintenance Procedures

The dam should be inspected annually with particular attention directed to the assessment of seepage problems and the condition of the concrete in the spillway and bridge.

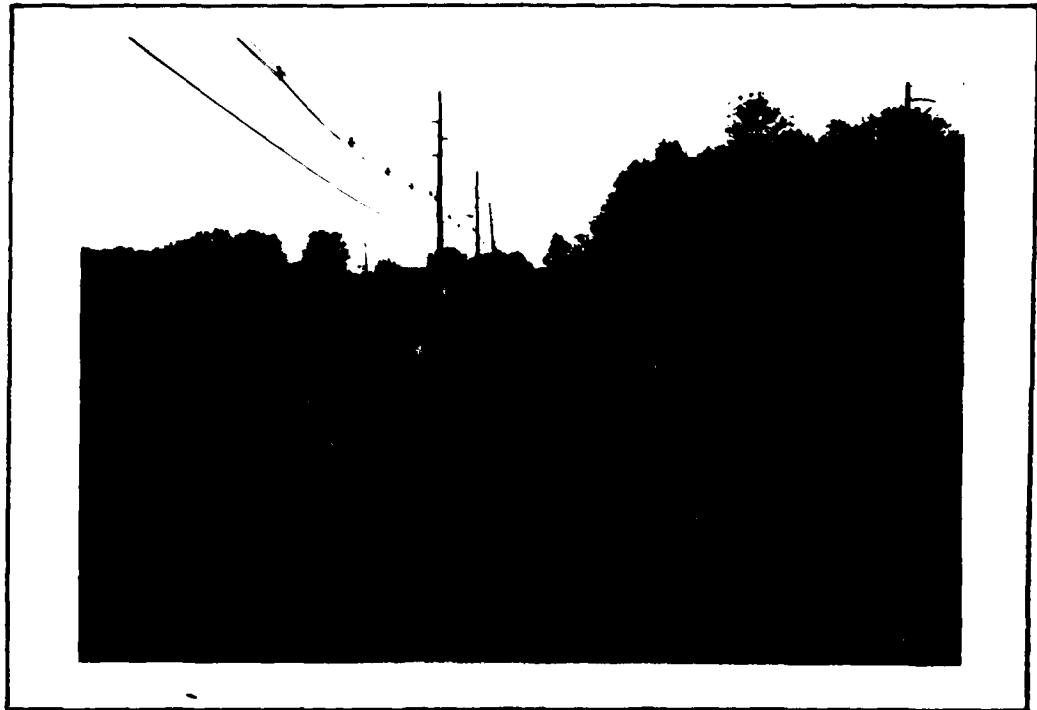
O'BRIEN & GERE ENGINEERS, INC.


John J. Williams, P.E.
Vice President
New Jersey Registration No. 24916

Date: 28 July 1981



OVERVIEW FROM THE LEFT ABUTMENT. NOTE THE CONCRETE HEADWALL FOR THE ABANDONED MILL RACE INLET. (5/6/81)



OVERVIEW FROM THE RIGHT ABUTMENT. (5/6/81)

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PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM
ETRA MILL POND DAM
INVENTORY NUMBER NJ 00298

1.1 General

a. Authority. This report is authorized by the Dam Inspection Act, Public Law 92-367, and has been prepared in accordance with contract #DACP61-80-D-0013 between O'Brien & Gere Engineers, Inc. and the United States Army Corps of Engineers, Philadelphia District.

b. Purpose of Inspection. The purpose of the inspection is to evaluate the structural and hydraulic condition of Etra Mill Pond Dam and appurtenant structures and to determine if the dam constitutes a hazard to human life or property.

1.2 Project Description (Based on information provided by the New Jersey Department of Environmental Protection (NJDEP) and supplemented by field observations.)

a. Description of Dam and Appurtenances. Etra Mill Pond Dam is an earth embankment about 300 feet long and 11 feet high. The crest width of the embankment averages about 25 feet. A paved roadway is constructed on the crest of the embankment. The average slope of the upstream face of the dam is about 2H:1V while the average slope of the downstream face of the dam is about 1H:1V.

An Ambursen reinforced concrete gravity spillway is constructed near the mid point of the embankment. Spillway discharge is passed through the embankment by means of a bridged opening. A 16-inch diameter reservoir drain gate is located in the upstream endwall of the spillway structure.

b. Location. Etra Mill Pond Dam is located in Mercer County approximately one mile southeast of Hightstown, New Jersey. The dam site is shown on the USGS Quadrangle entitled "Hightstown, New Jersey" at coordinates N40°15.2', W74°30.2'. A regional location map for Etra Mill Pond Dam is included as Figure 1, Appendix E.

c. Size Classification. Etra Mill Pond Dam has a maximum height of approximately 11 feet. The maximum storage at the low point of the top of the dam is estimated to be 114 acre feet. The dam is therefore classified as a "Small" size structure (height less than 40 feet, storage less than 1,000 acre feet).

d. Hazard Classification. No structures for human habitation in the downstream floodway would be affected by a failure of the dam. The extent of property damage as a result of dam failure is judged to be insignificant. The dam is therefore classified as a "Low" hazard potential structure.

e. Ownership. The dam is owned by East Windsor Township, New Jersey. Correspondence may be directed to: Ward Street, Municipal Building, East Windsor Township, New Jersey 08520, Attn: Mr. John Santouosso, Township Engineer.

f. Purpose of Dam. The dam was originally constructed to provide hydro-power for a mill. The impoundment is presently used for incidental recreation.

g. Design and Construction History. The original dam at the site was constructed sometime prior to 1930. No information relative to the design and construction of this dam is known to exist.

The application to reconstruct the dam to its present configuration was made in May, 1930. The Owner was Mr. Abraham Katz and the Engineer was John L. Weber, P.E. of Trenton, New Jersey. Construction began in August, 1930. The foundation was reported to consist of "gravel underlying clay." The spillway foundation was exposed and inspected by representatives of the New Jersey Water Policy Commission (NJWPC) in August, 1930. The NJWPC recommended several changes with regard to the foundation design.

A second NJWPC inspection of the dam was made on November 20, 1930. At this time it was noted that: 1) the concrete in the buttresses "contained many dry batches", 2) the blow-off pipe was located about 2 feet higher than shown on approved drawings and 3) that some leakage was noted under the spillway deck.

A NJWPC inspection of the dam was made on January 3, 1931. At this time, the pond was approximately half full. Seepage was noted at the base of the first buttress of the spillway (right side). Deposits of fines were observed at this location. The Owner was directed to dewater the impoundment and make appropriate repairs. A subsequent NJWPC inspection was made on March 16, 1931. The water surface was at the spillway crest and no leakage was observed. Acceptance of the completed structure was recommended.

The embankment was overtopped and breached in 1934 and in September, 1938. It was reported that the embankment was overtopped for about 10 hours and the maximum depth of flow over the road was about one foot in the 1938 event.

The September 1938 damage was repaired in January, 1939. The spillway crest elevation was reported to be lowered by 0.3 feet as recommended by the State. It is not known when the 1934 damage was repaired.

No additional information relative to design or construction history is available.

h. Normal Operating Procedures. According to the Owner's representative, Mr. John Santouosso, no operating procedures are currently in effect at this dam.

1.3 Pertinent Data

a. Drainage Area.

Square Miles 9.1

b. Discharge at Dam Site (cfs).

Low Point of Dam (Elev. 99.9) 310.

c. Elevation (Feet above NGVD).

Spillway Crest	98.6
Low Flood Notch	98.3
Design Top of Dam	101.6
Low Point Top of Dam (Surveyed)	99.9
Spillway Apron (Surveyed)	88.8

d. Reservoir Length (Feet).

Normal Pool (Elevation 98.3)	2,200
Low Point Top of Dam (Elevation 99.9)	3,000

e. Reservoir Storage (Acre Feet).

Normal Pool (Elevation 98.3)	66
Low Point Top of Dam (Elevation 99.9)	114

f. Reservoir Surface Area (Acres).

Normal Pool (Elevation 98.3)	21
Low Point Top of Dam (Elevation 99.9)	40

g. Dam.

Type	Earth Embankment
Length	+300 feet
Height	+11 feet
Top Width	+25 feet
Side Slopes (Upstream)	Average 2H:1V
Side Slopes (Downstream)	Average 1H:1V
Zoning	Unknown
Impervious Core	Unknown
Cutoff	Unknown
Grout Curtain	Unknown

h. Spillway.

Type	Box Inlet Drop Spillway Reinforced Concrete Ambursten Type
Length of Weir (Elevation 98.6)	49 Feet
Length of Low Flow Notch (Elevation 98.3)	12 Feet
Gate	16-inch diameter located in upstream spillway wall
Upstream Channel	Impoundment
Outlet Channel	Natural Stream

- i. Diversion and Regulating Structure. Diversion to former mill appears to be blocked. Size and closure method for diversion unknown.
- j. Reservoir Drain. The reservoir drain is reported to be a 16-inch diameter cast iron pipe and gate located through the base of the upstream wall of the spillway.

SECTION 2
ENGINEERING DATA

2.1 Design

a. Data Available. The engineering data provided by the New Jersey Department of Environmental Protection (NJDEP) includes the following:

1. Correspondence file initiated 1929.
2. Two design drawings of the dam entitled Mr. A. Katz, Dam, dated April, 1930.

2.2 Construction

Inspection and progress reports relative to the construction of the box inlet drop spillway reinforced concrete Ambursen type spillway, were provided by the NJDEP.

2.3 Operation

According to the Owner's representative, no operating program is currently in effect for the dam.

2.4 Evaluation

a. Availability. The engineering data used in preparing this report was provided by the NJDEP.

b. Adequacy. Based on a review of the material provided by the NJDEP, observations made during the field investigation and conversations with the Owner's representative, it appears that adequate information is available for a Phase I evaluation.

c. Validity. There appears to be no reason to question the validity of the data provided by the NJDEP.

SECTION 3

VISUAL INSPECTION

3.1 Findings

a. General. The field inspections of Etra Mill Pond Dam took place on April 30, May 6, May 13, and June 3, 1981. At the time of the inspections, the water surface was approximately 0.2 feet above the spillway crest low flow notch. The photographs which appear in Appendix D of this report were taken on May 6, 1981. No underwater areas were included in the inspection. The observations and comments of the field inspection team are included in the checklist which is Appendix B of this report. The overall appearance of the facility indicated that the dam and its appurtenances are inadequately maintained.

b. Dam. The vertical and horizontal alignment of the dam appears to be fair. No significant settlement or slope misalignment was noted. A survey of the vertical alignment of the top of the dam was made by the inspection team. The maximum variation in vertical alignment is about 1.7 feet. A sketch of the survey results is included in Appendix E, Sheet 5.

A low concrete wall is constructed along the upstream face of the embankment from the south abutment and extends for about 100 feet along the crest of the embankment. A concrete headwall structure is located at the northern end of this wall. The headwall is apparently a portion of the intake structure for an abandoned diversion system to a former mill. Timber gate guides are evident on this structure above the water level. The concrete wall and headwall appear to be in good condition.

The remainder of the upstream face of the dam which is constructed on a slope of about 2H:1V, is intermittently covered by uncontrolled vegetative growth consisting of reeds, grasses and brush. No appreciable erosion was observed in the areas where no vegetative cover exists.

The downstream face of the embankment is essentially flat in the abutment areas. However, in the vicinity of the spillway the slopes are approximating 1H:1V. The entire downstream face of the embankment is covered with dense uncontrolled vegetation including several large trees. Seepage was located in the toe area of the embankment on both sides of the spillway. On the left side of the spillway and about 10 feet from the channel, a spongy area was located. No puddled seepage was noted at this location. However, on the right side of the spillway, approximately 50 feet from the spillway, puddled water was detected. No flow was observed in the puddled water.

c. Appurtenant Structures. The alignment of the spillway structure is good. No cracks were evident in the structure; however, the concrete is spalled and reinforcing steel is exposed in at least two buttresses.

No cracking was noted in the bridge abutments. However, concrete tee beams of the road deck are spalled and reinforcing steel is exposed. According to Mr. John Santouosso, East Windsor Township Engineer, the allowable bridge load is restricted because of the defective beams.

According to information provided by NJDEP, the reservoir drain was constructed through the upstream endwall of the spillway. The operating mechanism was not evident during the inspections. The spillway crest was reportedly lowered during repairs made in 1939. However, no evidence of this modification are apparent.

d. Reservoir Area. The reservoir slopes are relatively flat and well covered with vegetation. No slope stability problems are apparent along the shoreline of the reservoir. A significant amount of sedimentation was observed in the impoundment.

e. Downstream Channel. The discharge from the spillway enters the natural channel downstream of the dam. The channel overbanks are heavily overgrown with brush and trees. Peddie Lake is located about 1.5 miles downstream. No inhabitable dwellings are located between Etra Mill Pond Dam and Peddie Lake that would be endangered by a failure of Etra Mill Pond Dam.

SECTION 4
OPERATIONAL FEATURES

4.1 Procedures

Based on a review of all available information and interviews with the Owner's representative, no operational procedures are associated with this dam.

4.2 Maintenance of Dam

According to the Owner's representative, maintenance is performed only on an as needed basis for this dam.

4.3 Maintenance of Operating Facilities

According to the Owner's representative, maintenance of operating facilities is performed only on an as needed basis for this dam.

4.4 Description of any Warning System in Effect

According to the Owner's representative, no warning system is in effect for this dam.

4.5 Evaluation of Operational Adequacy

It is not known if the reservoir drain is operational. No operating mechanism is evident. The diversion system appears to be abandoned and sealed off.

The dam is accessible for all weather conditions.

SECTION 5

HYDROLOGY AND HYDRAULICS

5.1 Evaluation of Features

a. Design Data. Based on a review of available information pertaining to the dam reconstruction in 1931, the drainage area contributing to Etra Mill Pond Dam is 9.09 square miles, the maximum depth of the pond is 10 feet and the surface area of the pool is 21 acres. The drainage basin has a maximum length of about 5.5 miles and a maximum width of about 2.5 miles. The topography ranges from a maximum of Elevation 350 to Elevation 98.3 at normal pool. The drainage area is a mixture of farmland and woodland with Perrineville being the only community within the basin.

For further information, refer to the calculations and computer printout included in Appendix C of this report.

b. Experience Data. According to the Owner's representative, no records of reservoir level or rainfall are maintained for this dam. Based on a review of available information, the dam was overtopped and breached in 1934 and 1938. During the storm of September 21 and 22, 1938, water was reported to have flowed at a depth of one foot over the top of the dam for at least 10 hours.

The time to completely drain the reservoir has been estimated to be approximately 1.2 days using the 16-inch diameter drain pipe.

c. Visual Observations. At the time of the inspections, it appeared that the spillway could perform as designed. The operational condition of the reservoir drain system could not be appraised and the abandoned diversion system appeared to be blocked off.

d. Overtopping Potential. Etra Mill Pond Dam is a "Small" size, "Low" hazard structure. Accordingly, the Spillway Design Flood (SDF) ranges from the fifty to the one-hundred year flood. The one-hundred year flood was selected as the SDF. The SDF hydrograph was developed and routed through the impoundment and dam with the starting water surface at the spillway crest, Elevation 98.3. The peak inflow and discharge rates during this event are about 1400 and 1390 cfs, respectively. The spillway is capable of discharging approximately 22 percent of the SDF prior to overtopping of the embankment. The SDF event overtops the embankment by about 0.8 feet for a period of 14.75 hours.

e. Spillway Adequacy. The spillway is incapable of discharging the SDF prior to overtopping; therefore, the spillway is judged to be "Inadequate."

SECTION 6

STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations. At the time of the inspections, the embankment appeared to be in fair condition. No evidence of slope instability was noted. However, areas of isolated seepage were located on both sides of the spillway at the downstream toe area. No deposits of fines were noted at either location.

The concrete spillway appeared to be in fair condition. Concrete was spalled and reinforcing steel exposed in at least two of the support buttresses. No misalignment was evident in the structure.

Concrete tee beams of the road deck are spalled and reinforcing steel is exposed in the highway bridge which is an integral part of the dam.

Based on the field inspection, Etra Lake Dam appears to be stable under any expected static loading conditions.

b. Design and Construction Data. Analyses of the buttressed reinforced concrete spillway were provided by the NJDEP. The analyses show that the resultant of forces is located within the middle third of the base width of the spillway section for a head of water one foot above the spillway crest.

c. Operating Records. According to the Owner's representative, no operating records are maintained for this dam.

d. Post Construction Changes. Refer to Section 1.2g.

e. Seismic Stability. The dam is located in Seismic Risk Zone 1 of the "Seismic Zone Map of Contiguous States." A dam located in Seismic Zone 1 is generally considered to be stable under any expected earthquake loading if it is stable under static loading conditions.

SECTION 7

ASSESSMENT, RECOMMENDATIONS AND PROPOSED REMEDIAL MEASURES

7.1 Dam Assessment

a. Evaluation. Based on the visual inspection, Etra Mill Pond Dam is judged to be in fair condition. Cover for the embankment slopes varies from being overgrown with brush and trees to bare unprotected earth. Seepage was detected near the downstream toe on both the left and right sides of the spillway. The concrete in the spillway structure is spalled and reinforcing steel is exposed in at least two of the buttresses.

The concrete in the bridge abutments is in fair condition. The concrete in the bridge beams is in poor condition. The highway bridge is an integral part of the dam.

The SDF selected for Etra Mill Pond Dam ("Small" size, "Low" hazard) is the 100 year flood event. A review of the results of the hydrologic and hydraulic analyses indicated that the spillway is capable of passing approximately 22 percent of the SDF prior to overtopping the embankment.

The operational condition of the reservoir drain is unknown.

b. Adequacy of Information. The information provided by the NJDEP, conversations with the Owner's representative and observations made during the field inspection provided adequate information for a Phase I evaluation.

c. Urgency. The remedial measures recommended in Section 7.2 should be initiated soon.

d. Necessity for further Investigation. Further detailed studies are not considered necessary because Etra Mill Pond Dam is a "Small" size, "Low" hazard dam.

7.2 Recommendations and Remedial Measures

The Owner should retain the services of a licensed professional engineer experienced in the design and construction of dams to assist in complying with the following recommendations and remedial measures.

The recommendations and remedial measures should be initiated soon.

a. Facilities

1. The embankment should be cleared of all brush and trees. Resulting voids should be backfilled with suitable compacted material. Controlled protective vegetation should be established on the embankment slopes.

2. The seepage downstream of the dam should be monitored regularly.
3. The capacity of the spillway should be increased to provide for safe passage of the SDF.
4. The concrete in the spillway and bridge should be repaired.
5. The reservoir drain should be inspected and repaired if necessary to insure satisfactory operation.
6. The diversion system to the former mill should be inspected to assess its suitability for use as an auxiliary reservoir drain.

b. Operation and Maintenance Procedures

The dam should be inspected annually with particular attention directed to the assessment of seepage problems and the condition of the concrete in the spillway and bridge.

APPENDIX

A

Check List Engineering Data
Design, Construction, Operation
Phase I

NAME OF DAM Etra Mill Pond Dam
ID # NJ 00298

Sheet 1 of 4

CHECK LIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

REMARKS

ITEM AS-BUILT DRAWINGS None made available.

REGIONAL VICINITY MAP

Refer to Appendix E, Figure 1.

CONSTRUCTION HISTORY

Refer to Sect. 1.2 g.

TYPICAL SECTIONS OF DAM

Refer to Appendix E, Figure 3.

OUTLETS - PLAIN

Refer to Appendix E, Figure 3.

DETAILS

CONSTRAINTS

DISCHARGE RATINGS None made available

RAINFALL/RESERVOIR RECORDS

None made available.

ITEM	REMARKS
DESIGN REPORTS	None made available.
GEOLOGY REPORTS	None made available.
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	Limited to information submitted with Dam Application.
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	None made available.
POST-CONSTRUCTION SURVEYS OF DAM	None made available.
BORROW SOURCES	No information available.

<u>ITEM</u>	<u>REMARKS</u>
MONITORING SYSTEMS	None.
MODIFICATIONS	Refer to Section 1.2 g.
HIGH POOL RECORDS	None made available.
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None made available.
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	Refer to Section 1.2 g.
MAINTENANCE OPERATION RECORDS	None made available.

ITEM	REMARKS
SPILLWAY PLATE	
SECTIONS	Refer to Appendix E, Figure 3.
DETAILS	
OPERATING EQUIPMENT PLANS & DETAILS	No information was made available.
MISCELLANEOUS	

APPENDIX

B

Check List

Visual Inspection

Phase I

CHECK LIST
VISUAL INSPECTION
PHASE 1

Sheet 1 of 7

Name Dam	Etra Mill Pond Dam	County	Mercer	State	New Jersey	National ID #
Type of Dam	Earth Embankment	Hazard Category	Low			NJ 00298
Date(s) Inspection	May 6 & 13, 1981	Weather	Cloudy/with rain	Temperature	65°	
	June 3, 1981				(4/30/81)	(4/30/81)

Pool Elevation at Time of Inspection 98.5 ± M.S.L. Tailwater at Time of Inspection 90 ± M.S.L.

Inspection Personnel:

L.R. Beck	Lee DeHeer (6/3/81)
R.E. Horvath	
J.F. Rauschkolb	R.E. Horvath
	Recorder

Remarks:

The inspection team was accompanied by Mr. John Santoussos, East Windsor Township Engineer on 4/30/81 and Mr. Peter Niyen, Assistant Township Engineer on May 6, 1981

Sheet 2 of 7		
<u>EMBANKMENT</u>	<u>OBSERVATIONS</u>	<u>REMARKS OR RECOMMENDATIONS</u>
<u>VISUAL EXAMINATION OF</u>		
<u>SURFACE CRACKS</u>	No cracking was noted in the embankment.	
<u>UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE</u>	No evidence of movement was noted in the vicinity of the embankment toe.	
<u>SLoughing OR Erosion OF EMBANKMENT AND ABUTMENT SLOPES</u>	None noted.	
<u>VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST</u>	The vertical and horizontal alignment of the crest is fair.	
<u>RIPRAP FAILURES</u>	No riprap is in place.	Riprap should be installed on the upstream face of the embankment for erosion protection.

EMBANKMENT

Sheet 3 of 7

<u>VISUAL EXAMINATION OF</u>	<u>OBSERVATIONS</u>	<u>REMARKS OR RECOMMENDATIONS</u>
------------------------------	---------------------	-----------------------------------

JUNCTION OF EMBANKMENT
AND ABUTMENT, SPILLWAY
AND DAM

No movement or cracking was noted.

ANY NOTICEABLE SEEPAGE

Seepage was evident on both sides of the spillway. A "spongy" area was located about 10 feet to the left of the spillway channel. "Ponded" water was located about 50 feet to the right of the channel. No flow was observed in the puddled water.

These conditions should be observed during periodic inspections to detect any changes in flow quantity or quality.

STAFF GAGE AND RECORDER

None.

DRAINS

None.

Reservoir Drain
OUTLET WORKS

Sheet 4 of 7

<u>VISUAL EXAMINATION OF</u>	<u>OBSERVATIONS</u>	<u>REMARKS OR RECOMMENDATIONS</u>
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	N/A	
INTAKE STRUCTURE	Submerged.	
OUTLET STRUCTURE		According to available information, the outlet is constructed through the spillway structure. However, due to flow conditions, the structure was not observed.
OUTLET CHANNEL		The outlet channel is the spillway channel.
EMERGENCY GATE		16-inch diameter gate located in upstream spillway wall.

UNGATED SPILLWAY

Sheet 5 of 7

<u>VISUAL EXAMINATION OF</u>	<u>OBSERVATIONS</u>	<u>REMARKS OR RECOMMENDATIONS</u>
CONCRETE WEIR	The concrete weir appear to be in good condition. The concrete in at least two of the buttresses is spalled and reinforcing steel is exposed.	The concrete should be repaired.
APPROACH CHANNEL	Impoundment.	
DISCHARGE CHANNEL	Discharge from the spillway passes through the embankment by means of a bridged opening in the embankment. The flow enters the natural downstream channel downstream of the bridge.	
BRIDGE AND PIERS	The concrete in the bridge structure appears to be in poor condition.	The concrete should be repaired.

RESERVOIR

Sheet 6 of 7

REMARKS OR RECOMMENDATIONS

OBSERVATIONS

VISUAL EXAMINATION OF

SLOPES

The reservoir slopes are relatively flat and well covered with vegetation. No slope stability problems are apparent along the shoreline of the reservoir.

SEDIMENTATION

A significant degree of sedimentation was observed in the impoundment.

Limits the storage capacity of the reservoir.

DOWNSTREAM CHANNEL

VISUAL EXAMINATION OF		OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)		The natural channel downstream of the dam appears to be relatively free of debris and obstructions. The overbanks are heavily overgrown with brush and trees.	
SLOPES		The downstream channel slope and channel sideslopes are relatively flat. Peddie Lake is located about 1.5 miles downstream.	
APPROXIMATE NO. OF HOUSES AND POPULATION		No structures for human habitation in the downstream floodway would be affected by a failure of the dam. The extent of property damage as a result of dam failure is judged to be insignificant. The dam is therefore classified as a "Low" hazard potential structure.	

APPENDIX

C

Hydrologic & Hydraulic Data

ETRA MILL POND DAM
APPENDIX C
HYDROLOGIC AND HYDRAULIC
ENGINEERING DATA

TABLE OF CONTENTS

	<u>Sheet No.</u>
Snyder Coefficients	1
One Hundred Year Storm Development	2 through 4
Typical Channel Section Upstream of Etra Mill Pond	5
Stage - Discharge Computations, Etra Mill Pond Dam	6
Stage - Area Computations, Etra Mill Pond Dam	7
Stage - Discharge and Stage - Area Computations, Perrineville Lake Dam	8
Drawdown Calculations	9
HEC-1, Dam Safety Version, Computer Printout	10 through 14



O'BRIEN & GERE

SUBJECT	ETRA MILL POND DAM		SHEET	BY	DATE	JOB NO
	1		JFR	5-28-81	6/8/81	1800-006-114

✓ 6/8/81

SNYDER COEFFICIENTS

$$\begin{aligned} C_t &= 2.0 \\ C_p &= 0.6 \end{aligned} \quad \left. \begin{aligned} C_t &= 2.0 \\ C_p &= 0.6 \end{aligned} \right\} \text{Determined by Philadelphia C.D.E.}$$

PERRINEVILLE LAKE

$$T_p = C_t (L \cdot L_{ca})^{0.3}$$

$$L = 2.04 \text{ mi.}, L_{ca} = 1.09 \text{ mi.}$$

$$\begin{aligned} T_p &= 2.0 (2.04 \times 1.09)^{0.3} \\ &= 2.54 \text{ hours} \end{aligned}$$

ETRA MILL POND

$$T_p = C_t (L \cdot L_{ca})^{0.3}$$

$$L = 6.06 \text{ mi.}, L_{ca} = 2.32 \text{ mi.}$$

$$T_p = 2.0 (6.06 \times 2.32)^{0.3}$$

$$= 4.42 \text{ hours}$$



OBRIEN & GERE

SUBJECT	ETRA MILLS POND DAM		SHEET	BY	DATE	JOB NO
			2	JFR	6-1-81	1B00-006-114

188 6/8/81

ONE HUNDRED YEAR STORM DEVELOPMENTRAINFALL FOR 100 YEAR RETURN *

DURATION	RAINFALL
30 MIN.	2.4"
1 HR.	3.2"
2 HR.	3.9"
3 HR.	4.3"
6 HR.	5.2"
12 HR.	6.2"
24 HR.	7.2"

* FROM TP-40, U.S. WEATHER BUREAU

THE FOLLOWING HYPOTHETICAL HYETOGRAPH WAS DEVELOPED USING THE SCS METHOD OF RAINFALL DISTRIBUTION. DATA FOR THE STORM WAS ACQUIRED FROM AN ACCUMULATED RAINFALL-DURATION CURVE. THE 24-HOUR MASS CURVE WAS DIVIDED INTO 15-MINUTE INTERVALS TO OBTAIN THE CORRESPONDING RAINFALL INCREMENTS.



O'BRIEN & GERE

OBJECT

ETRA MILLS POND DAM

SHEET

3

BY

JFR

DATE

6-1-81

JOB NO

1800-006-114

6/4/81

100 YR. STORM DISTRIBUTION

TIME INTERVAL (HOURS)	FROM	TO	RAINFALL INCREMENT (INCHES)	NUMBER OF INCREMENTS
0	4 3/4	4 3/4	.02	19
4 3/4	7 1/4	7 1/4	.03	10
7 1/4	8	8	.04	3
8	9	9	.05	4
9	9 1/2	9 1/2	.06	2
9 1/2	10	10	.07	2
10	10 1/2	10 1/2	.08	1
10 1/2	10 3/4	10 3/4	.10	1
10 3/4	11	11	.12	1
11	11 1/4	11 1/4	.14	1
11 1/4	11 1/2	11 1/2	.20	1
11 1/2	11 3/4	11 3/4	.34	1
11 3/4	12	12	.90	1
12	12 1/4	12 1/4	1.50	1
12 1/4	12 1/2	12 1/2	.41	1
12 1/2	12 3/4	12 3/4	.20	1
12 3/4	13	13	.16	1
13	13 1/4	13 1/4	.13	1
13 1/4	13 1/2	13 1/2	.10	1
13 1/2	13 3/4	13 3/4	.09	1
13 3/4	14 1/4	14 1/4	.08	2
14 1/4	14 3/4	14 3/4	.07	2
14 3/4	15 1/4	15 1/4	.06	2
15 1/4	16	16	.05	3
16	17	17	.04	4
17	19 1/2	19 1/2	.03	10
19 1/2	24	24	.02	18

7.20"

96



O'BRIEN & GERE

OBJECT	ETRA MILLS POND DAM	SHEET	4	BY	JFR	DATE	6-02-81	JOB NO	1800-006-114
--------	---------------------	-------	---	----	-----	------	---------	--------	--------------

✓ 6/9/81

PEAK DISCHARGE FOR 100-YR. STORM

REFERENCE: SPECIAL REPORT 38 "MAGNITUDE AND FREQUENCY OF FLOODS IN NEW JERSEY WITH EFFECTS OF URBANIZATION", NEW JERSEY D.E.P., 1974.

$$Q_{100} = 136 \cdot A^{0.84} \cdot S^{0.26} \cdot St^{-0.51} \cdot I^{0.14}$$

ETRA MILLS

A = drainage area = 6.3 sq.mi.

S = main channel slope, ft. per mi.
= $\frac{160 - 100}{4.55} = 13.2 \frac{\text{ft.}}{\text{mi.}}$

St = surface storage index
= 2.5, avg. for Raritan River Basin

I = index of manmade impervious cover
= 5.2, avg. for Raritan River Basin

$$Q_{100} = 136 (6.3)^{0.84} (13.2)^{0.26} (2.5)^{-0.51} (5.2)^{0.14} = \underline{985} \text{ cfs}$$

PERRINEVILLE

A = 2.8 sq.mi.

S = $\frac{255 - 165}{1.53} = 58.7 \frac{\text{ft.}}{\text{mi.}}$

$$Q_{100} = 136 (2.8)^{0.84} (58.7)^{0.26} (2.5)^{-0.51} (5.2)^{0.14} = \underline{735} \text{ cfs}$$



O'BRIEN & GERE

UBJECT

ETRA MILLS POND DAM

5

BY

JFR

DATE

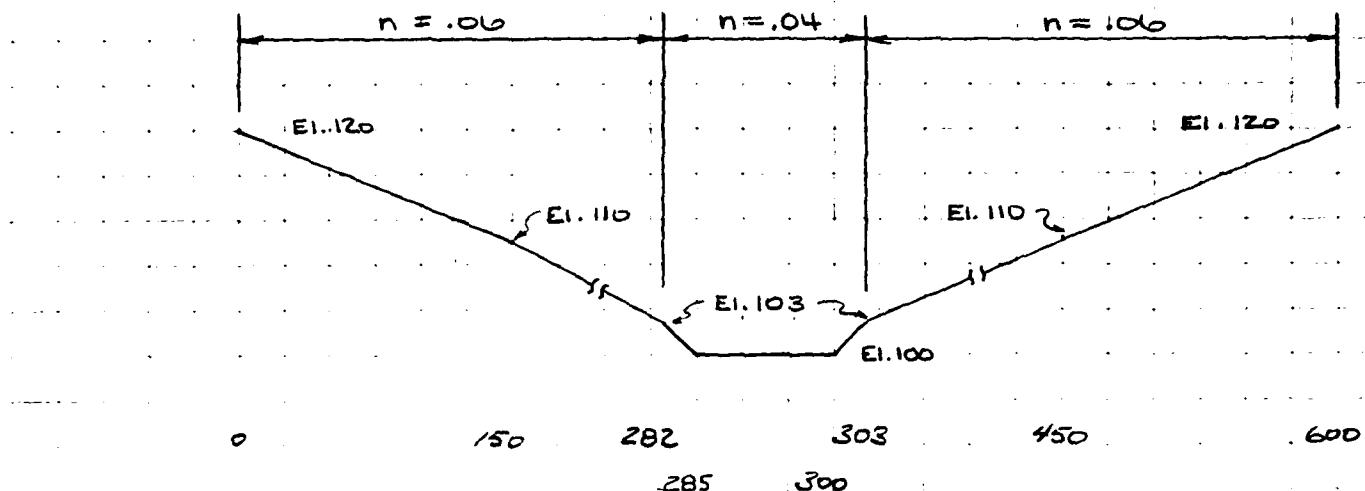
6-01-81

JOB NO

1800-006-114

✓
6/9/81

TYPICAL CHANNEL SECTION UPSTREAM OF ETRA MILLS POND



REACH LENGTH = 24,500 ft.

$$\text{CHANNEL SLOPE} = \frac{150 - 100}{24,500} = 0.002 \frac{\text{ft}}{\text{ft}}$$



OBRIEN & GERE

SUBJECT

Etra Mills Pond Dam	SHEET	BY	DATE	JOB NO
	6	REH	5/27/81	1800-000.114

At Etra MillsStage-Discharge + Spillway: $C = 3.43$ (uncorrected)Ref: Hid. Design of the Box-Inlet Drop Spillway
Agriculture Hbk #301
6/9/81

WSE	H_1 (ft)	H_2 (ft)	L_1 (ft)	L_2 (ft)	W/W	correction factor for Head for B/W	C
98.3	0	0	12	49	10	—	—
99.3	1	0.7			106	.82	2.78
100.3	2	1.7			111	.88	2.99
101.3	3	2.7			117	.92	3.12
102.3	4	3.7			122	.94	3.19
103.3	5	4.7			128	.96	3.26
104.3	6	5.7			133	.97	3.29
105.3	7	6.7			139	.99	3.36
106.3	8	7.7			144	.99	3.36
107.3	9	8.7			15	1.00	3.39

WSE	H_1	H_2	$Q_1 = C(12)H_1^{3/2}$	$Q_2 = C(49)H_2^{3/2}$	Q TOTAL
98.3	0	0	0 cfs	0 cfs	0 cfs
99.3	1	.7	33	00	113
100.3	2	1.7	101	325	426
101.3	3	2.7	195	678	873
102.3	4	3.7	306	1112	1418
103.3	5	4.7	437	1628	2065
104.3	6	5.7	580	2134	2774
105.3	7	6.7	747	2855	3602
106.3	8	7.7	912	3518	4430
107.3	9	8.7	1098	4263	5361

For embankment overtopping use $Q = CLH^{3/2}$ $C = 2.6$; $L = 400$ feet

embankment Crest elevation = 99.93.



O'BRIEN & GERE

OBJECT

Etra Mills Pond Dam

SHEET

7
ZEH

DATE

5/27/81

JOB NO

1803006-112

v/f 6/9/81

A + Etra Mills

Stage - Area

<u>Stage</u>	<u>Surface Area</u>
98.3	21 acres
100.0	40 acres
120.0	468 acres



OBRIEN & GERE

SUBJECT

Etra Mill Pond Dam	sheet	by	Date	Job No
	8	REH	5/27/81	1800.006.110

V86 6/9/81

Upstream Dam @ Perrineville

STAGE - Discharge $C = CLH^{3/2}$ $C = 3.6, L = 30$ feetStage 14 Q (cfs)

164	10	10
165	11	108
166	12	395
167	13	561
168	14	864
169	15	1207
170	16	1587
171	17	2000
172	18	2444
173	19	2916

For embankment overtopping use $CLH^{3/2}$ $C = 2.6, L = 450'$
embankment crest elev = 170STAGE - AREAStageSurface Area

164 (normal pool)	13.7 Acres
170	44 Acres
180	92 Acres



O'BRIEN & GERE

SUBJECT

ETIRA MILLS POND DAM

SHEET

9 JFR

DATE

7-27-81 1800-006-114

DRAWDOWN ANALYSIS16" ϕ drain pipe at El. 88.9; Normal Pool, El. 98.2

$$t = \frac{\pi}{Q}$$

$$\pi = 3450.8923 (h_2 - h_1)^3 \text{ ft}^3; \text{ By Integration}$$

$$Q = A \sqrt{2gH} = 11.205 H^{1/2} \text{ cfs}$$

<u>Δ DEPTH</u>	<u>$\Delta \pi$ (ft³)</u>	<u>H_{Avg} (ft)</u>	<u>Q (cfs)</u>	<u>t (sec)</u>
98.30 - 97.36	776,753	8.93	33.5	23,187
97.36 - 96.42	621,976	7.59	31.7	19,621
96.42 - 95.48	484,396	7.05	29.8	16,255
95.48 - 94.54	364,013	6.11	27.7	13,141
94.54 - 93.60	260,829	5.17	25.5	10,229
93.60 - 92.66	174,841	4.23	23.0	7,602
92.66 - 91.72	106,051	3.29	20.3	5,224
91.72 - 90.78	54,459	2.35	17.2	3,166
90.78 - 89.84	20,064	1.41	13.3	1,509
89.84 - 88.90	<u>2866</u>	.47	7.7	<u>372</u>
Σ 2,866,248				<u>100,305 sec</u>

$$t_{TOTAL} = \frac{100,305 \text{ sec}}{86400} = \underline{\underline{1.2 \text{ days}}}$$

FLOOD-HYDROGRAPH PACKAGE--(HEC-1)
DAM SAFETY VERSION JULY 1978
LAST MODIFICATION 01 AFR 80

NATIONAL DAM SAFETY PROGRAM
 EXTRA HILLS POND DAM
 100-YEAR STORM ROUTING
 RUNOFF TO FERRINEVILLE LAKE

42	0	0	0	0.3
43	0	-96	0	
44	T			
45	W	44.2	0.60	
46	X	-1.5	-0.05	
47	K1	2	LAKE-2	0
			COMBINE-RUNOFF-TO-ETRA	0
48	K1	1	1	OUTFLOW-FROM-PERRINEVILLE-AT-ETRA
49	K1	0	0	0
50	K1	0	0	0
			OUTFLOW-FROM-ETRA-MILLS-FOND-DAM	1
				1
				-1
				-57

540

ଓনিয়েশ হৰ্ষগোপীনাম

NOTE ON FROM EFFICIENT VILLE NAME

AW OUTFLOW IS - 617. AT TIME - 16:00 HOURS - HYDROGRAPH ROUTING
PERRINEVILLE OUTFLOW ROUTED TO ETRA

STAGE	OUTFLOW	STORAGE
100.00	0.00	0.00
95.53	27.01	9.50
90.53	86.07	49.73
84.51	101.05	75.42
79.51	102.11	64.74
74.51	103.16	59.73
69.51	113.68	54.74
64.51	114.74	49.73
59.51	126.63	44.74
54.51	126.63	39.73
49.51	126.63	34.74
44.51	126.63	29.73
39.51	126.63	24.74
34.51	126.63	19.73
29.51	126.63	14.74
24.51	126.63	9.73
19.51	126.63	4.74
14.51	126.63	0.00
9.50	20.25	32.52
4.50	48.44	139.84
0.00	86.07	173.18
0.00	98.93	101.98
0.00	102.11	102.11
0.00	113.68	113.68
0.00	114.74	114.74
0.00	121.72	221.73
0.00	126.63	226.63
0.00	126.63	231.73
0.00	126.63	236.63
0.00	126.63	241.73
0.00	126.63	246.63
0.00	126.63	251.73
0.00	126.63	256.63
0.00	126.63	261.73
0.00	126.63	266.63
0.00	126.63	271.73
0.00	126.63	276.63
0.00	126.63	281.73
0.00	126.63	286.63
0.00	126.63	291.73
0.00	126.63	296.63
0.00	126.63	301.73
0.00	126.63	306.63
0.00	126.63	311.73
0.00	126.63	316.63
0.00	126.63	321.73
0.00	126.63	326.63
0.00	126.63	331.73
0.00	126.63	336.63
0.00	126.63	341.73
0.00	126.63	346.63
0.00	126.63	351.73
0.00	126.63	356.63
0.00	126.63	361.73
0.00	126.63	366.63
0.00	126.63	371.73
0.00	126.63	376.63
0.00	126.63	381.73
0.00	126.63	386.63
0.00	126.63	391.73
0.00	126.63	396.63
0.00	126.63	401.73
0.00	126.63	406.63
0.00	126.63	411.73
0.00	126.63	416.63
0.00	126.63	421.73
0.00	126.63	426.63
0.00	126.63	431.73
0.00	126.63	436.63
0.00	126.63	441.73
0.00	126.63	446.63
0.00	126.63	451.73
0.00	126.63	456.63
0.00	126.63	461.73
0.00	126.63	466.63
0.00	126.63	471.73
0.00	126.63	476.63
0.00	126.63	481.73
0.00	126.63	486.63
0.00	126.63	491.73
0.00	126.63	496.63
0.00	126.63	501.73
0.00	126.63	506.63
0.00	126.63	511.73
0.00	126.63	516.63
0.00	126.63	521.73
0.00	126.63	526.63
0.00	126.63	531.73
0.00	126.63	536.63
0.00	126.63	541.73
0.00	126.63	546.63
0.00	126.63	551.73
0.00	126.63	556.63
0.00	126.63	561.73
0.00	126.63	566.63
0.00	126.63	571.73
0.00	126.63	576.63
0.00	126.63	581.73
0.00	126.63	586.63
0.00	126.63	591.73
0.00	126.63	596.63
0.00	126.63	601.73
0.00	126.63	606.63
0.00	126.63	611.73
0.00	126.63	616.63
0.00	126.63	621.73
0.00	126.63	626.63
0.00	126.63	631.73
0.00	126.63	636.63
0.00	126.63	641.73
0.00	126.63	646.63
0.00	126.63	651.73
0.00	126.63	656.63
0.00	126.63	661.73
0.00	126.63	666.63
0.00	126.63	671.73
0.00	126.63	676.63
0.00	126.63	681.73
0.00	126.63	686.63
0.00	126.63	691.73
0.00	126.63	696.63
0.00	126.63	701.73
0.00	126.63	706.63
0.00	126.63	711.73
0.00	126.63	716.63
0.00	126.63	721.73
0.00	126.63	726.63
0.00	126.63	731.73
0.00	126.63	736.63
0.00	126.63	741.73
0.00	126.63	746.63
0.00	126.63	751.73
0.00	126.63	756.63
0.00	126.63	761.73
0.00	126.63	766.63
0.00	126.63	771.73
0.00	126.63	776.63
0.00	126.63	781.73
0.00	126.63	786.63
0.00	126.63	791.73
0.00	126.63	796.63
0.00	126.63	801.73
0.00	126.63	806.63
0.00	126.63	811.73
0.00	126.63	816.63
0.00	126.63	821.73
0.00	126.63	826.63
0.00	126.63	831.73
0.00	126.63	836.63
0.00	126.63	841.73
0.00	126.63	846.63
0.00	126.63	851.73
0.00	126.63	856.63
0.00	126.63	861.73
0.00	126.63	866.63
0.00	126.63	871.73
0.00	126.63	876.63
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0.00	126.63	886.63
0.00	126.63	891.73
0.00	126.63	896.63
0.00	126.63	901.73
0.00	126.63	906.63
0.00	126.63	911.73
0.00	126.63	916.63
0.00	126.63	921.73
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0.00	126.63	931.73
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0.00	126.63	941.73
0.00	126.63	946.63
0.00	126.63	951.73
0.00	126.63	956.63
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0.00	126.63	971.73
0.00	126.63	976.63
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0.00	126.63	986.63
0.00	126.63	991.73
0.00	126.63	996.63
0.00	126.63	1001.73
0.00	126.63	1006.63
0.00	126.63	1011.73
0.00	126.63	1016.63
0.00	126.63	1021.73
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0.00	126.63	1031.73
0.00	126.63	1036.63
0.00	126.63	1041.73
0.00	126.63	1046.63
0.00	126.63	1051.73
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0.00	126.63	1061.73
0.00	126.63	1066.63
0.00	126.63	1071.73
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0.00	126.63	1181.73
0.00	126.63	1186.63
0.00	126.63	1191.73
0.00	126.63	1196.63
0.00	126.63	1201.73
0.00	126.63	1206.63

MAXIMUM STAGE IS 104.8
FLOW 0.00 27.01 86.0/ 173.18 321.27 763.82 1539.24 3302.48
6591.51 6177.20 6041.64 60198.93 12663.17 15448.39 18568.42 20307.01 25867.59 30073.49

84/12

SUB-AREA RUNOFF COMPUTATION

RUNOFF TO ETRA MILLS FOND

1STAGE ICIMP ICCON ITAPE JFRT INAME IStage IAuto

LAKE-2 0 0 0 0 0 1 0 0

HYDROGRAPH DATA

THNG TUHG TAFAA SNAF TSFLC TSFC

0 1 6.30 0.00 6.30 0.00

LOSS DATA

LROFT STRK TBLIN RTDOL ERAN STRSK RT10K

0 0.00 1.00 0.00 1.00 0.00

STRTL CNSTL ALSMX RTIMP

0 0.00 0.00 0.00 0.00

RECEDITION DATA

START= -1.50 ORCSN= -.05 RTIOR= 2.00

UNIT HYDROGRAPH END-OF-PERIOD ORDINATES, LAG=

4.38 HOURS, CP= .61 VOL= .99

29, 60, 97, 139, 183, 230, 279, 329,

429, 506, 534, 556, 571, 579, 579, 569,

513, 484, 457, 431, 407, 385, 363, 343,

273, 257, 243, 229, 217, 204, 191, 182,

153, 145, 137, 129, 122, 115, 109, 103,

86, 82, 77, 73, 69, 65, 61, 58,

52, 49, 46, 43, 41, 39, 37, 34,

29, 27, 26, 24, 22, 21, 19, 18,

16, 15, 14, 13, 12, 11, 10, 10,

9, 8, 7, 6, 6, 6, 5,

END-OF-PERIOD FLOW

MO./DA HR./MN PERIOD RAIN EXCS LOSS COMP Q

SUM 7.20 2.45 4.75 39802.

COMBINE HYDROGRAPHS

1STAGE ICIMP ICCON ITAPE JFRT INAME IStage IAuto

LAKE-2 2 0 0 0 0 1 0 0

HYDROGRAPH ROUTING

OUTFLOW FROM ETRA MILLS POND DAM

1STAGE ICIMP ICCON ITAPE JFRT INAME IStage IAuto

DAKE-2 1 0 0 0 0 1 0 0

ROUTING DATA

LOSS AVG ISME IOPF IPMP LSTR

0.0 0.00 0.00 1 1 0 0 0

NSTDE NSTDE LA0 MNSKK X TSK STORA ISPRAT

1 0 0.000 0.000 0.000 -98. -1

STAGE 98.30 99.30 100.30 101.30 102.30 103.30 104.30 105.30

FLOW 0.00 113.00 426.00 873.00 1418.00 2065.00 2774.00 3602.00

CAPACITY 0. 66. 117. 4416.

ELEVATION 89. 98. 100. 120.

PEEL SPWD DDMN EXPV ELEV COOL CAREA EXFL

DAM DATA

Sh 13

RUNOFF SUMMARY. AVERAGE FLOW IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
AREA IN SQUARE MILE(SQUARE KILOMETERS)

		PEAK	6-HOUR	24-HOUR	72-HOUR	AREA
	HYDROGRAPH AT 1-LANE-1	747.1	542.1	207.1	69.1	2.80
		(21.15)	(15.36)	(5.86)	(1.97)	(7.25)
ROUTE-TO	DAM-1	617.7	504.1	207.1	70.1	2.80
		(17.48)	(14.28)	(5.85)	(1.97)	(7.25)
ROUTE-TO	LAKE-2	467.1	424.1	204.1	70.1	2.80
		(13.21)	(12.01)	(5.77)	(1.97)	(7.25)
	HYDROGRAPH AT LAKE-2	981.7	839.1	408.1	138.1	6.30
		(27.78)	(23.75)	(11.54)	(3.91)	(16.32)
2-COMBINED	LAKE-2	1397.7	1248.1	611.1	208.1	9.10
		(39.55)	(35.33)	(17.30)	(5.88)	(23.57)
ROUTE-TO	DAM-2	1389.7	1240.1	604.1	208.1	9.10
		(39.33)	(35.12)	(17.10)	(5.89)	(23.57)

SUMMARY OF DAM SAFETY ANALYSIS

PLAN	INITIAL ELEVATION	SPILLWAY CREST	TOP-OF-DAM
	164.00	164.00	170.00
	STORAGE	0.	165.
	OUTFLOW	0.	150?
	RATIO OF RESERVOIR DEPTH	MAXIMUM STORAGE	MAXIMUM DURATION
	FMF W.S.ELEV	OVER DAM AC-FT	OVER TOP CFS
			MAX OUTFLOW HOURS
			FAILURE HOURS
1.00	167.19	0.00	65.
			617. 0.00 16.00 0.00
			STATION LAKE-2
	RATIO	MAXIMUM FLOW, CFS	MAXIMUM STAGE, FT
			TIME
			OF FAILURE HOURS
1.00	467.1	404.8	10.50
	PLAN 1	INITIAL ELEVATION	SPILLWAY CREST
		98.30	98.30
		STORAGE	99.93
		OUTFLOW	
	RATIO OF RESERVOIR DEPTH	MAXIMUM STORAGE	MAXIMUM DURATION
	FMF W.S.ELEV	OVER DAM AC-FT	OVER TOP CFS
			MAX OUTFLOW HOURS
			FAILURE HOURS
1.00	100.74	.81	149. 1389. 14.75 17.50 0.00

OK 14

APPENDIX

D

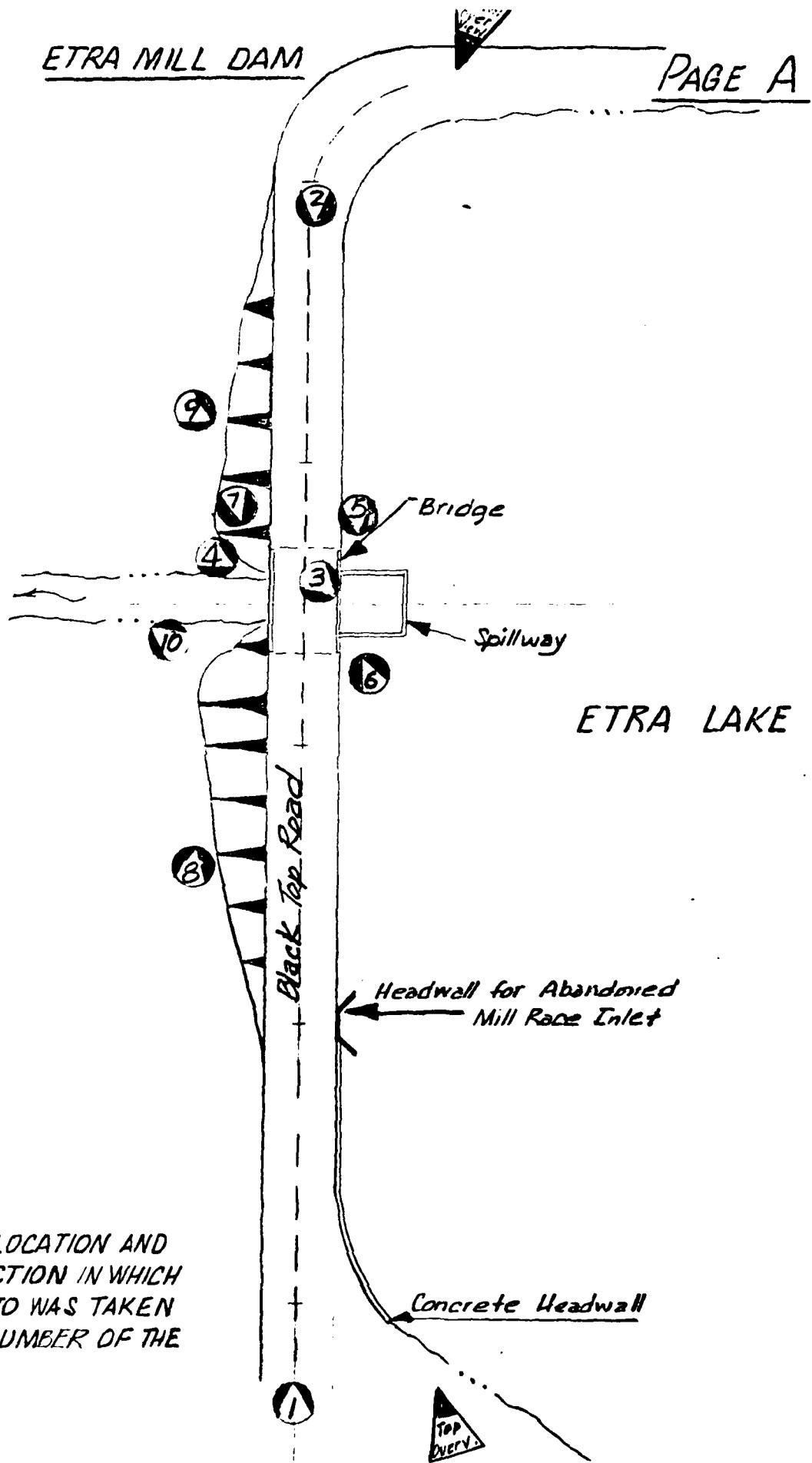
Photographs

APPENDIX D
SELECTED PHOTOGRAPHS OF THE SITE

	<u>Page No.</u>
Site Plan	A
<u>PHOTOGRAPH NO.</u>	
1. Paved roadway on the embankment crest as viewed from the left abutment. (5/6/81)	1
2. Paved roadway on the embankment crest as viewed from the right abutment. (5/6/81)	1
3. The spillway and impoundment. Note the low flow notch. (5/6/81)	2
4. Spillway structure looking upstream under the highway bridge. (5/6/81)	2
5. Left side of spillway structure. (5/6/81)	3
6. Right Side of spillway structure. (5/6/81)	3
7. Downstream side of bridge showing deteriorated concrete. (5/6/81)	4
8. Downstream face of the embankment. (5/6/81)	4
9. Seepage located at toe of embankment, right side of spillway. (5/6/81)	5
10. Downstream channel. (5/6/81)	5

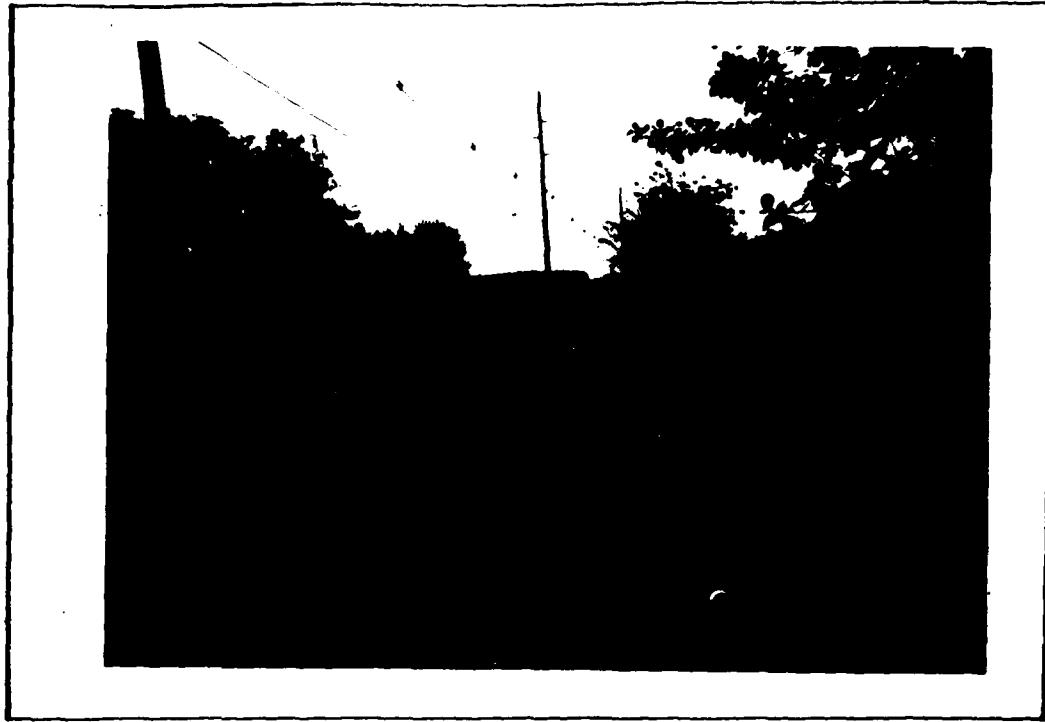
ETRA MILL DAM

PAGE A



LEGEND

1 THE LOCATION AND DIRECTION IN WHICH EACH PHOTO WAS TAKEN AND THE NUMBER OF THE PHOTO.



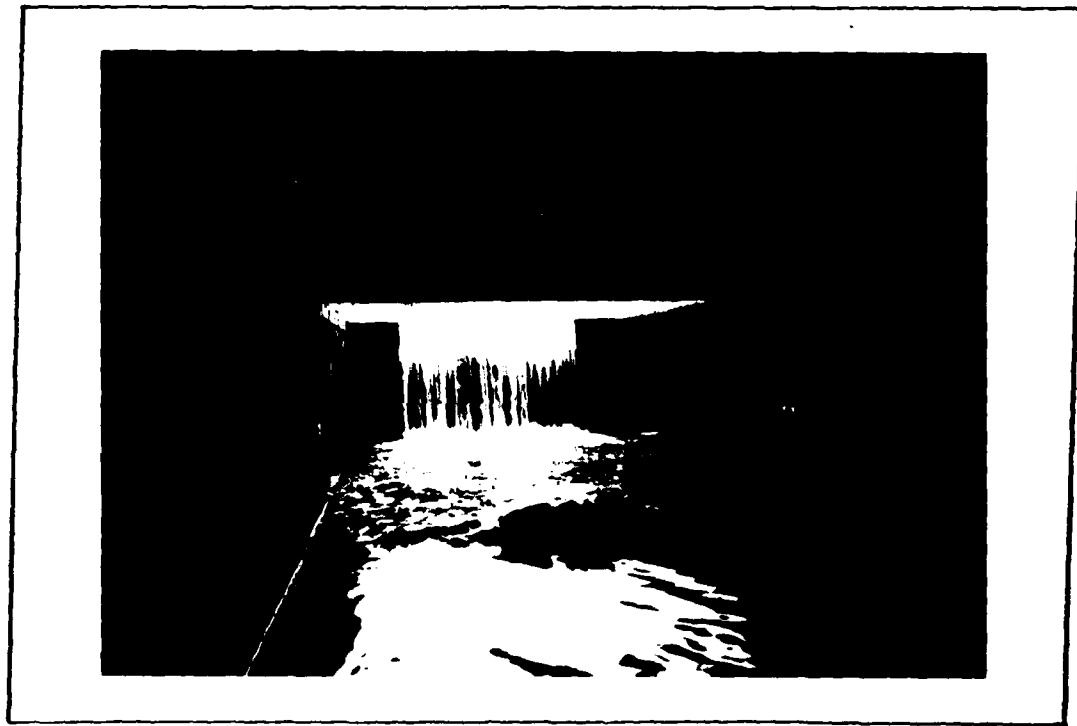
1. PAVED ROADWAY ON THE EMBANKMENT CREST AS VIEWED FROM THE LEFT ABUTMENT. (5/6/81)



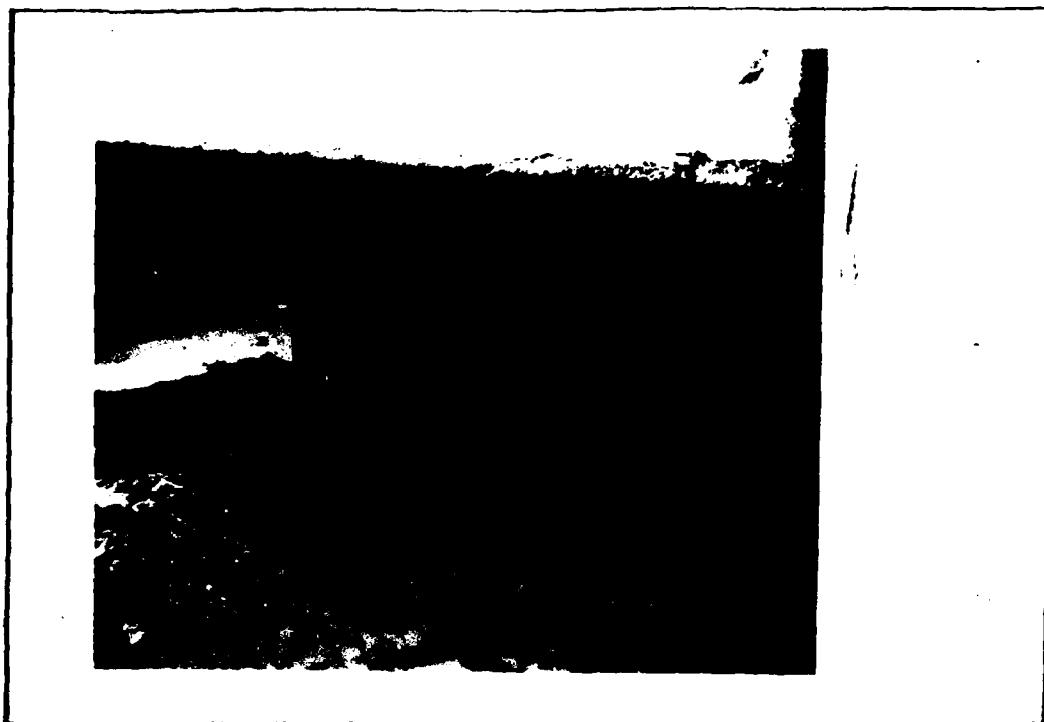
2. PAVED ROADWAY ON THE EMBANKMENT CREST AS VIEWED FROM THE RIGHT ABUTMENT. (5/6/81)



3. THE SPILLWAY AND IMPOUNDMENT. NOTE THE LOW FLOW NOTCH.
(5/6/81)



4. SPILLWAY STRUCTURE LOOKING UPSTREAM UNDER THE HIGHWAY
BRIDGE. (5/6/81)



5. LEFT SIDE OF SPILLWAY STRUCTURE. (5/6/81)



6. RIGHT SIDE OF SPILLWAY STRUCTURE. (5/6/81)



7. DOWNSTREAM SIDE OF BRIDGE SHOWING DETERIORATED CONCRETE.
(5/6/81)



8. DOWNSTREAM FACE OF THE EMBANKMENT. (5/6/81)



9. SEEPAGE LOCATED AT TOE OF EMBANKMENT, RIGHT SIDE OF SPILLWAY.
(5/6/81)



10. DOWNSTREAM CHANNEL. (5/6/81)

APPENDIX

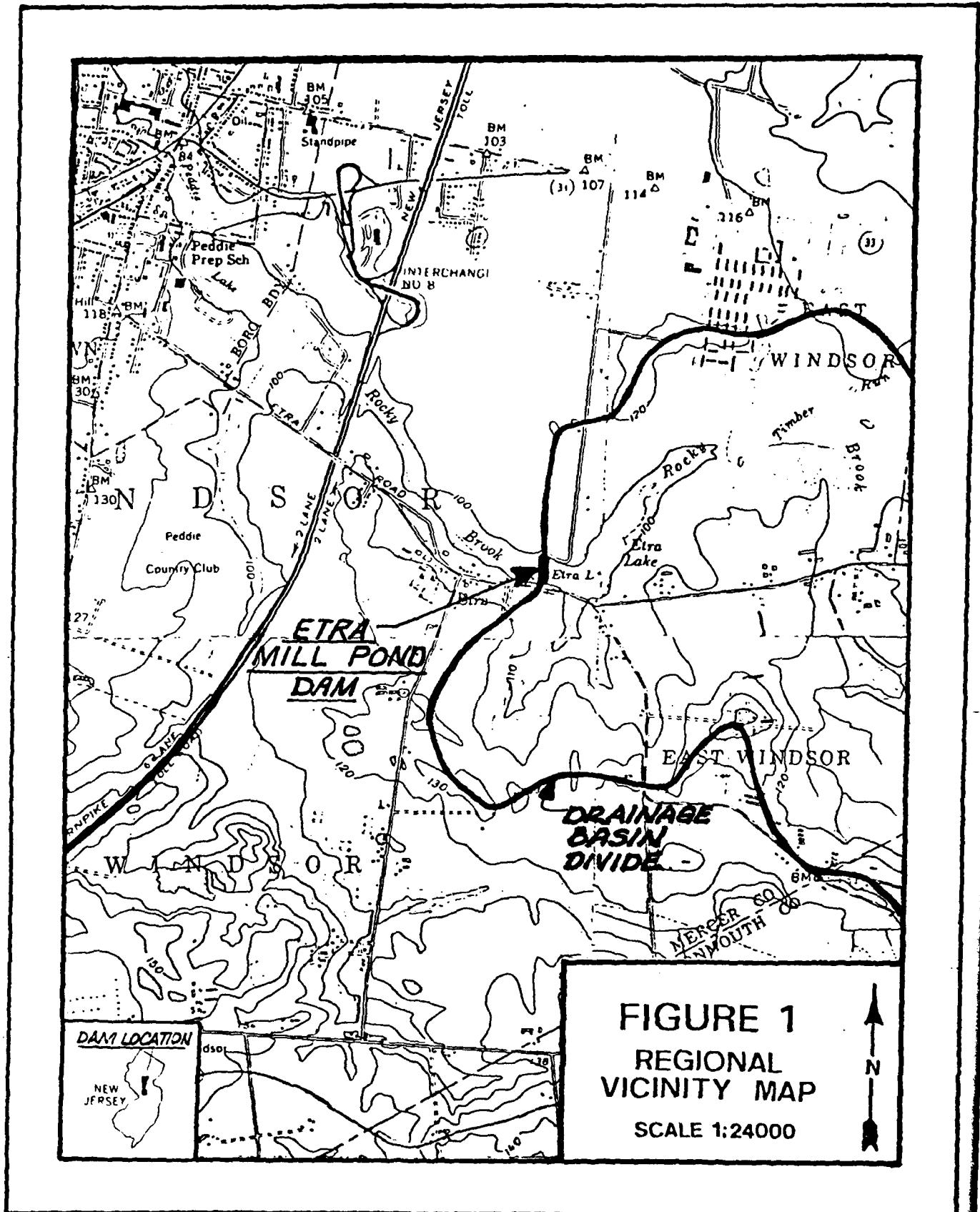
E

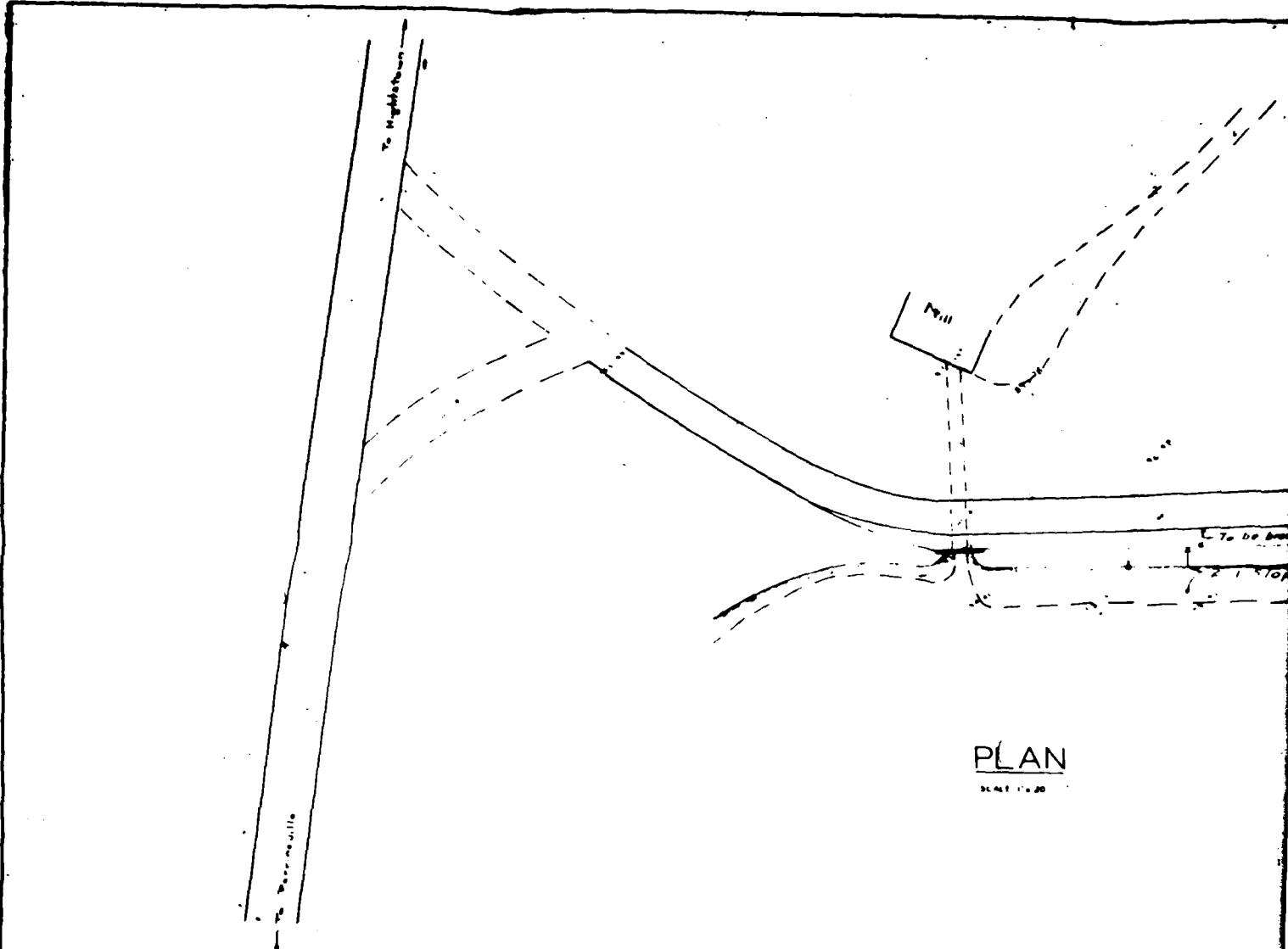
Drawings

ETRA MILL POND DAM
APPENDIX E
DRAWINGS

TABLE OF CONTENTS

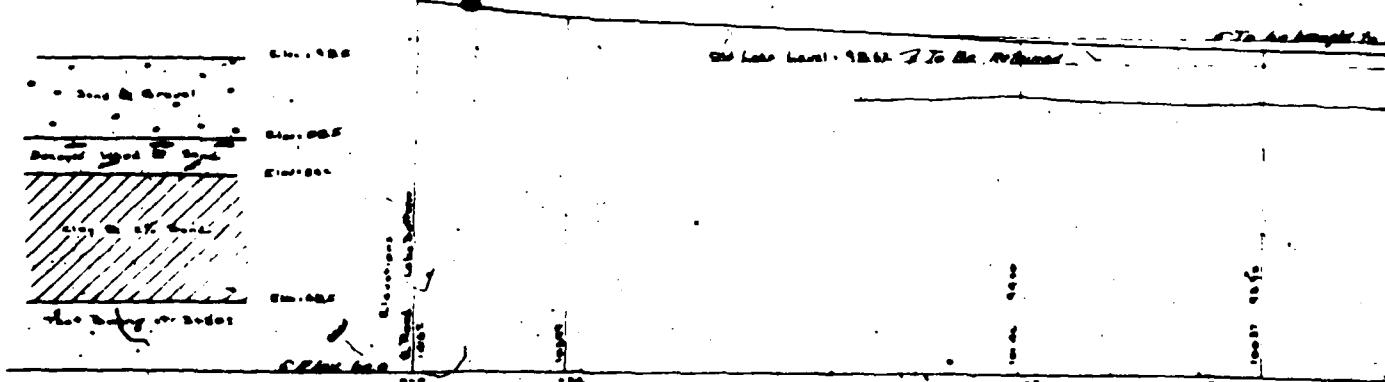
	<u>Sheet No.</u>
Regional Vicinity Map, Figure 1	1
Plan and Profile of Dam, 1930 Drawings	2
Spillway, 1930 Drawings	3
Plan View - Sketch of Dam, May 1981	4
Survey Vertical Crest Alignment, May 1981	5





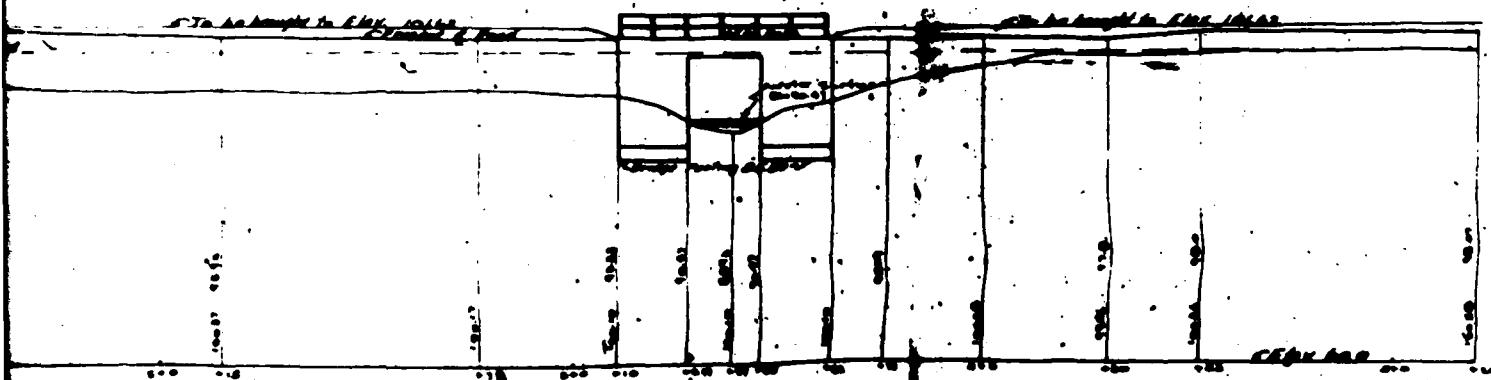
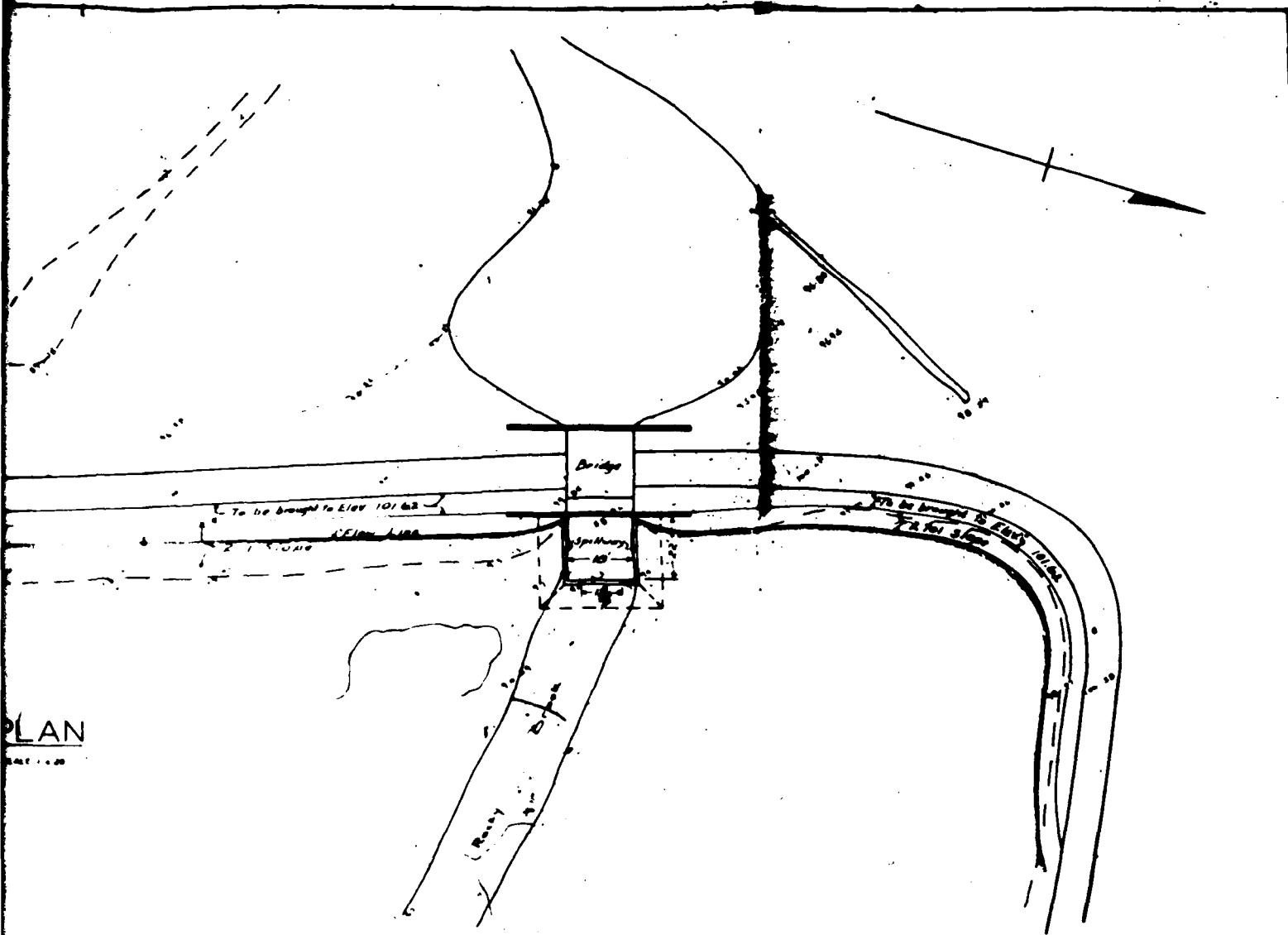
PLAN

Scale 1:1000



PROFILE

Scale 1:1000

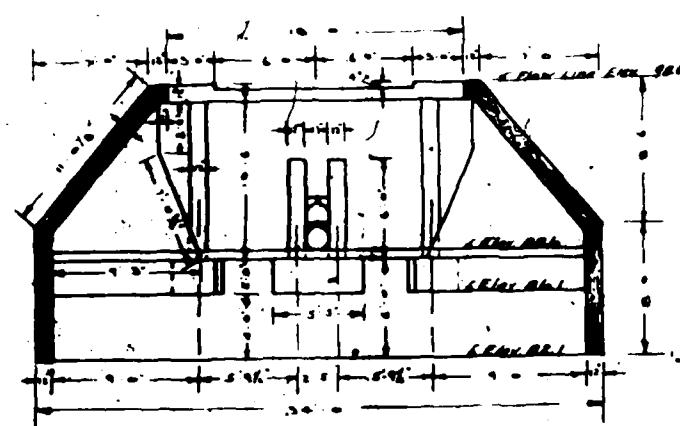
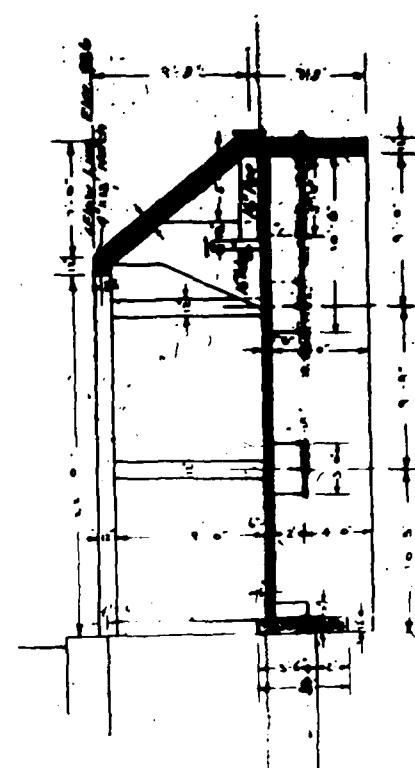
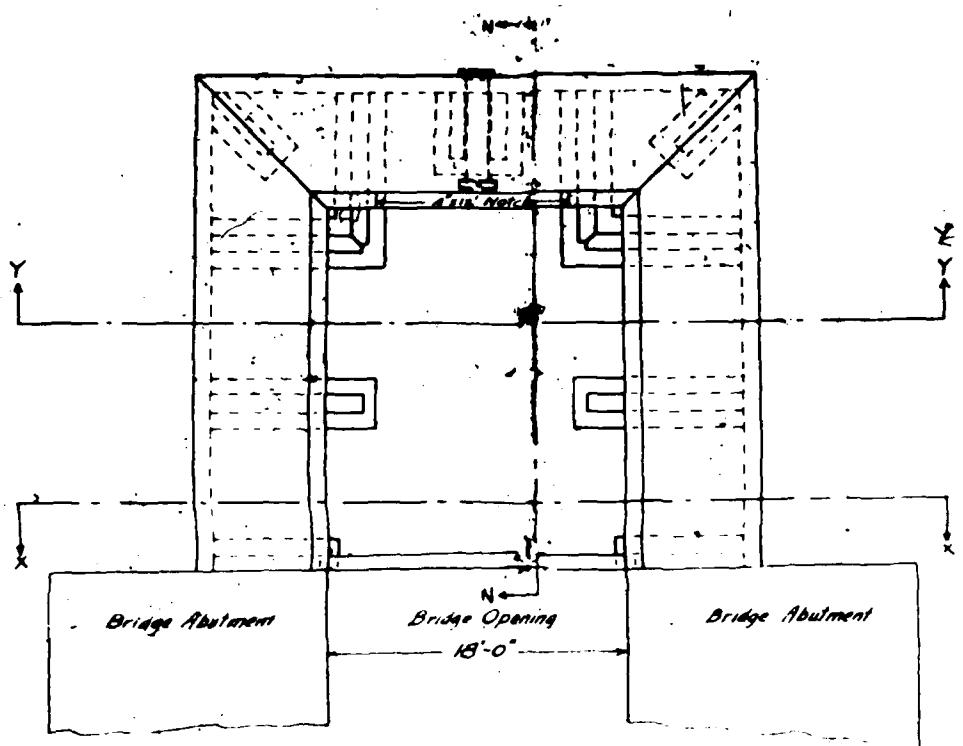


PROFILE

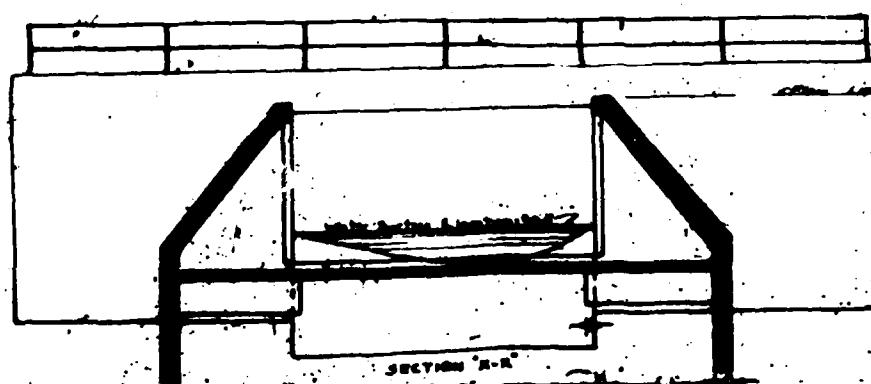
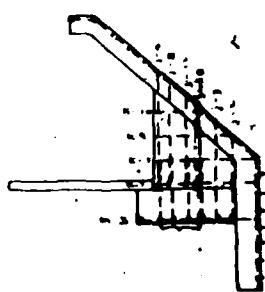
M.A. KATZ
DAM
JOHN L. WEBER, INC.

SHEET 2

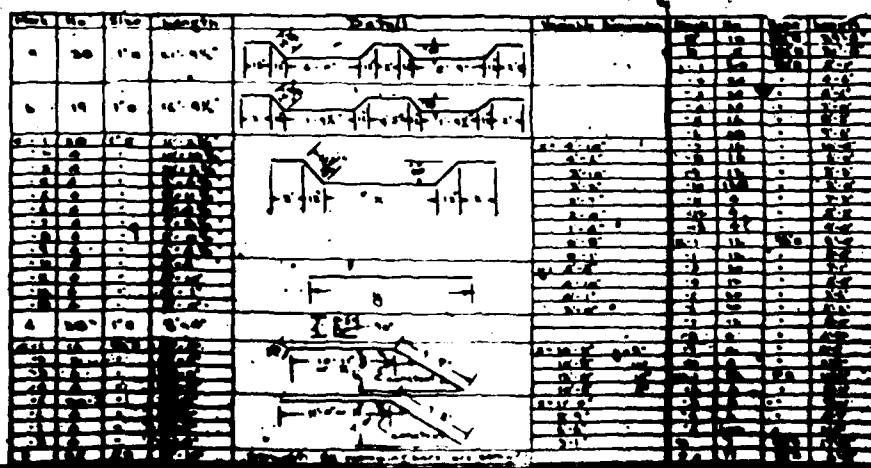
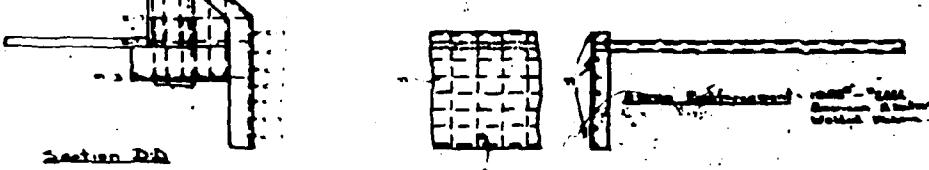
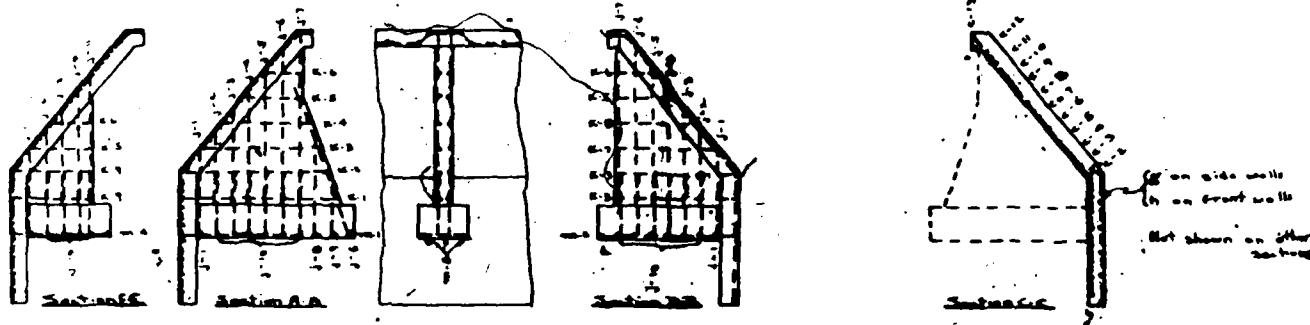
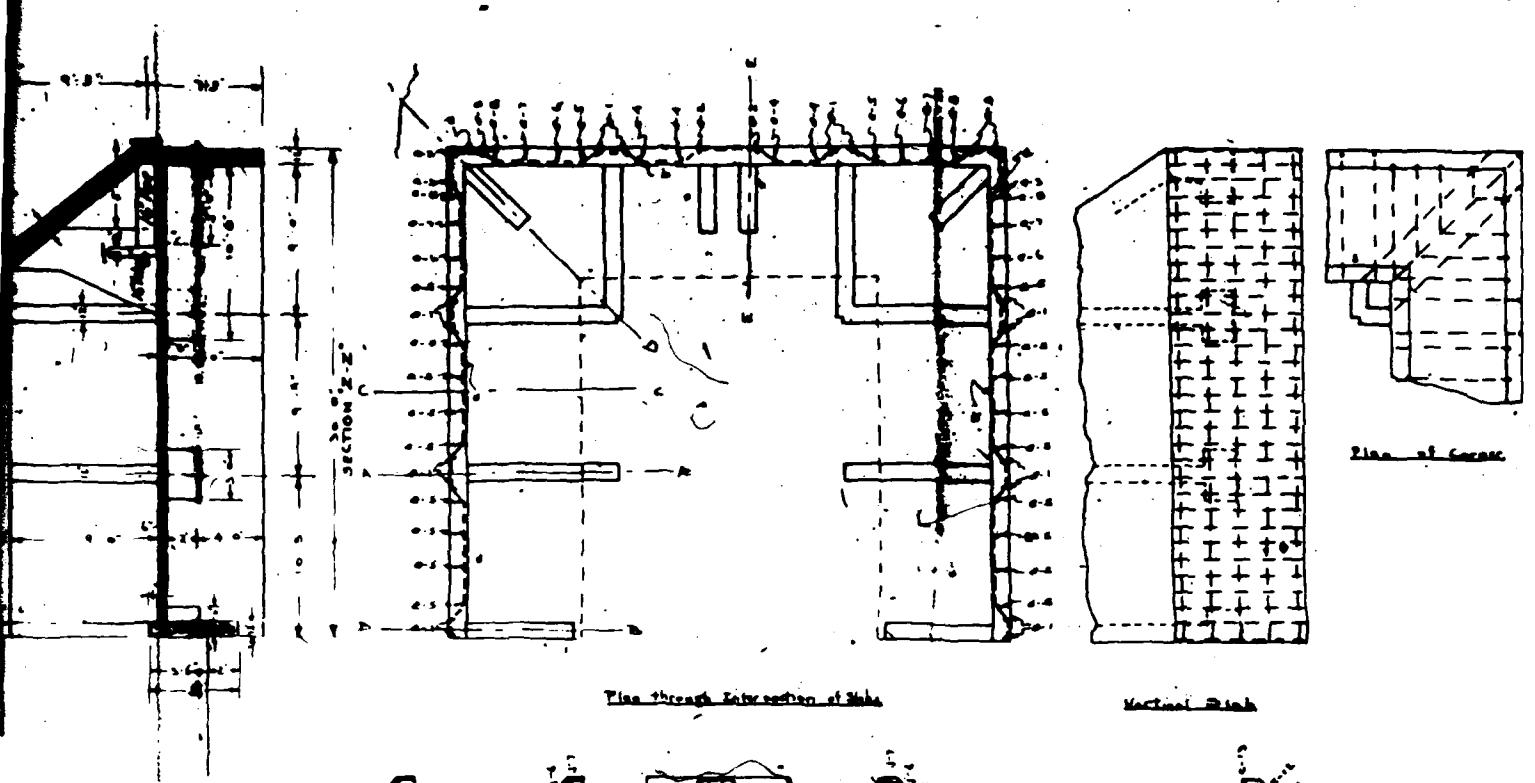
2



Weld Holes to be placed in Areas 10 & 11
Weld Holes and Inspection Points to be
located as directed by the Engineer



Part	No.	Size	Length
1	20	1/8	16'-0"
2	18	1/8	16'-0"
3	20	1/8	16'-0"
4	20	1/8	16'-0"
5	20	1/8	16'-0"
6	20	1/8	16'-0"
7	20	1/8	16'-0"
8	20	1/8	16'-0"
9	20	1/8	16'-0"
10	20	1/8	16'-0"
11	20	1/8	16'-0"
12	20	1/8	16'-0"
13	20	1/8	16'-0"
14	20	1/8	16'-0"
15	20	1/8	16'-0"
16	20	1/8	16'-0"
17	20	1/8	16'-0"
18	20	1/8	16'-0"
19	20	1/8	16'-0"
20	20	1/8	16'-0"
21	20	1/8	16'-0"
22	20	1/8	16'-0"
23	20	1/8	16'-0"
24	20	1/8	16'-0"
25	20	1/8	16'-0"
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27	20	1/8	16'-0"
28	20	1/8	16'-0"
29	20	1/8	16'-0"
30	20	1/8	16'-0"
31	20	1/8	16'-0"
32	20	1/8	16'-0"
33	20	1/8	16'-0"
34	20	1/8	16'-0"
35	20	1/8	16'-0"
36	20	1/8	16'-0"
37	20	1/8	16'-0"
38	20	1/8	16'-0"
39	20	1/8	16'-0"
40	20	1/8	16'-0"
41	20	1/8	16'-0"
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65	20	1/8	16'-0"
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67	20	1/8	16'-0"
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69	20	1/8	16'-0"
70	20	1/8	16'-0"
71	20	1/8	16'-0"
72	20	1/8	16'-0"
73	20	1/8	16'-0"
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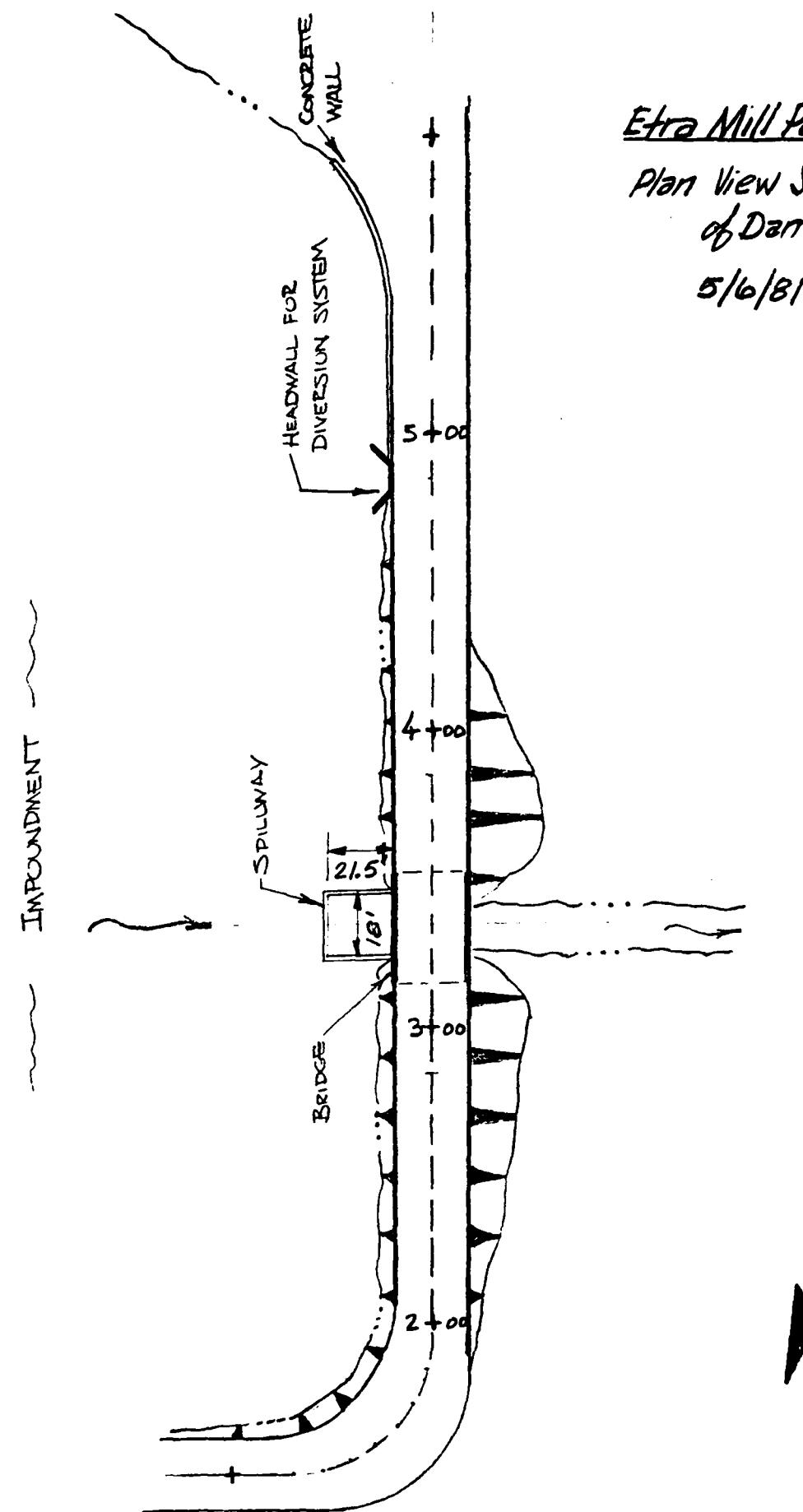
SPILLWAY

MR. A. KATZ

DAM

JOHN L. WEISS, INC.

SHEET 3



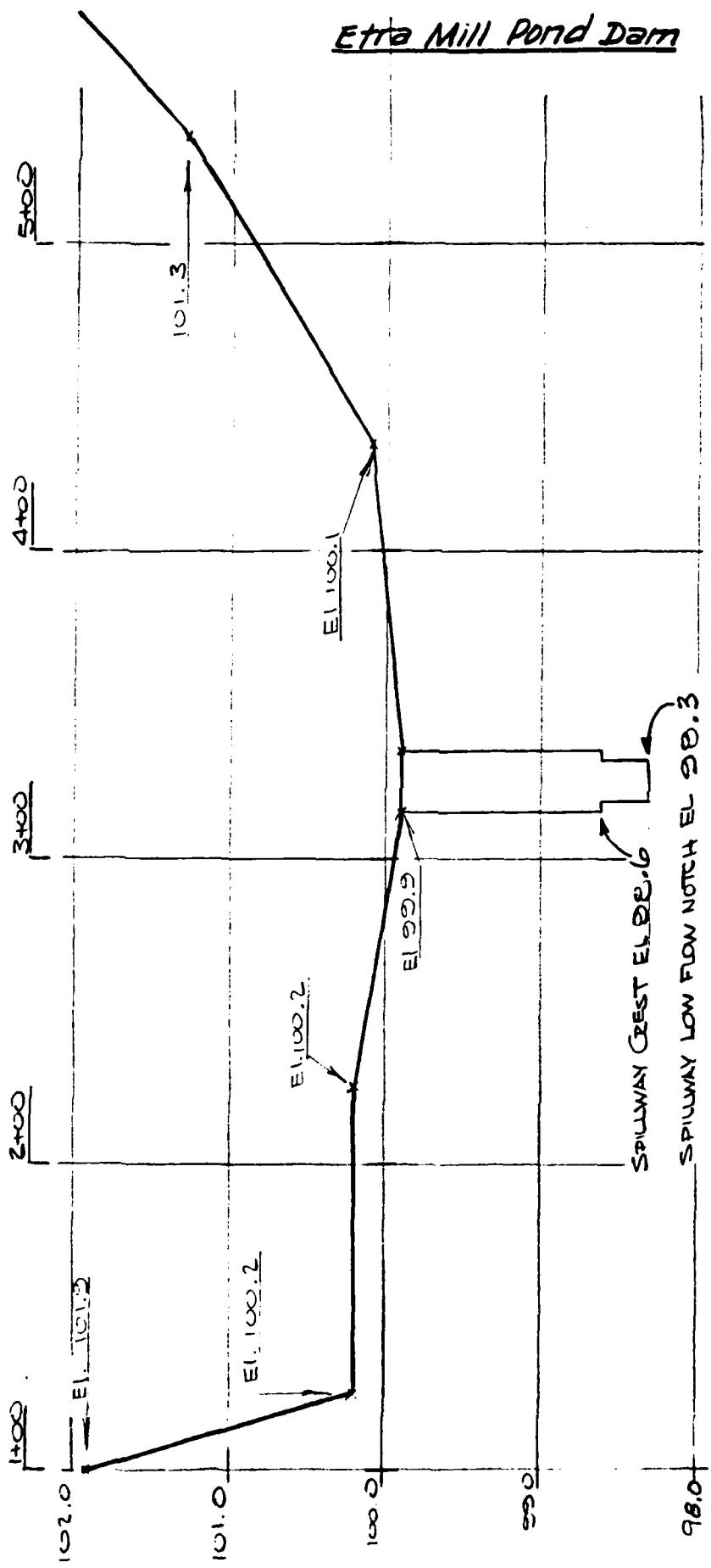
Etra Mill Pond Dam
Plan View Sketch
of Dam
5/6/81

Sh 4

Etta Mill Pond Dam

SURVEY - VERTICAL CREST ALIGNMENT

May 6, 1900



sh 5

APPENDIX

F

Site Geology

SITE GEOLOGY

ETRA LAKE DAM

Etra Lake Dam is located in Mercer County within the northwesterly limits of the Atlantic Coastal Plain physiographic province. The project rests on medium to fine grained marine sediments of Cretaceous age represented by the Englishtown formation. Younger sediments of Quaternary age, represented by the sands and gravels of the Pennsauken formation, mantle the underlying marine formation forming caps on terraces and topographic highs. The Englishtown formation strikes N.65°E. and dips gradually to the southeast.

The outcrop area where granular in nature may serve as recharge for the Englishtown aquifer used in New Jersey as a water supply source.

Bedrock is estimated to be about 300' feet below ground surface and to consist of highly weathered Paleozoic metamorphics.

